City of Carlsbad

1635 Faraday Av Carlsbad, CA 92008

Plan Check Revision

Permit No:PCR04115

Building Inspection Request Line (760) 602-2725

Job Address:

6030 AVENIDA ENCINAS CBAD

Permit Type:

Reference #:

Project Title:

Valuation:

PCR

Parcel No:

\$0.00

Lot #:

Construction Type: NEW

Status: Applied: ISSUED

07/13/2004

Entered By: Plan Approved:

RMA 09/17/2004

Issued: Inspect Area: 09/17/2004

TOYOTA-STEEL CAR PORT-DEFERRED

SUBMITTAL

Owner:

Applicant:

HAMANN CONST.

475 W. BRADLEY AV **EL CAJON, CA 92020**

Plan Check Revision Fee

Additional Fees

\$240.00 \$0.00

Total Fees:

\$240.00

Total Payments To Date:

\$0.00

Balance Due:

\$240.00

1396 09/17/04 0002 01

CGP

240.00

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Inspector:	
III SUCCIOI.	

Date: _

Clearance: .

NOTICE: Please take NOTICE that approval of your project includes the "Imposition" of fees, dedications, reservations, or other exactions hereafter collectively referred to as "fees/exactions." You have 90 days from the date this permit was issued to protest imposition of these fees/exactions. If you protest them, you must follow the protest procedures set forth in Government Code Section 66020(a), and file the protest and any other required information with the City Manager for processing in accordance with Carlsbad Municipal Code Section 3.32.030. Failure to timely follow that procedure will bar any subsequent legal action to attack, review, set aside, void, or annul their imposition.

You are hereby FURTHER NOTIFIED that your right to protest the specified fees/exactions DOES NOT APPLY to water and sewer connection fees and capacity changes, nor planning, zoning, grading or other similar application processing or service fees in connection with this project. NOR DOES IT APPLY to any fees/exactions of which you have previously been given a NOTICE similar to this, or as to which the statute of limitations has previously otherwise expired.

PERMIT APPLICATION CALL (BO4090 GECARE)



PLAN CHECK NO. CROHIS

, Emmer Air EloArion	Jug 00 - 13		TEAN CHECK NO.) Cr W (11)
CITY OF CARLSBAD BUIL	DING DEPARTMENT		EST. VAL.	
1635 Faraday Ave., Carlsb		200	Plan Ck. Deposit	10 A
,	,	FORNIT	Validated By	, \
		•	Date 7/3/	04
REPROJECT INFORMATION		MANNI TOYOTA	XCOOLS BAD	
Address (include Bldg/Suite #)	ncinas	Business Name (at t	this address)	
				
Legal Description	Lot No. Subdivisio	n Name/Number	Unit No. Phase No.	Total # of units
Assessor's Parcel #	Existing Use		Proposed Use	
Description of Work	SQ. FT. ₽	₩of Stories A	# of Bedrooms	# of Bathrooms
STEEL CARF	ort - defer	red Subn	Hal	(619)440-7421
2 CONTACT PERSON (If different fro	om applicant)	neer Way	El Chim 9702	O SHOW THE
Name	Address	Cily	State/Zip Telepho	
Contractor Contractor	Agent tor Contractor - Owner	C Agent for Owner		
Name	Address	City	State/Zip Telepho	one #
AS GEPROPERTY/OWNER DESIGN SAFEKE		grego salajn post te diligija i 1947.		
Name	Address	City	State/Zip Telepho	one #
5 EECONTRACTOR COMPANY NAMI		NAME OF THE PARTY		
(Sec. 7031.5 Business and Professions issuance, also requires the applicant for	Code: Any City or County which re	equires a permit to construct, alte	er, improve, demolish or repair any	structure, prior to its
(Chapter 9, commending with Section	7000 of Division 3 of the Business	s and Professions Code) or that	he is exempt therefrom, and the	basis for the alleged
exemption. Any violation of Section 70	31.5 by any applicant for a permit s	ubjects the applicant to a civil pe	inalty of not more than five hundred $CaMM = 92030$	d dollars (\$500)). 519 440 -7424
Name	Address	2 Gity	State/Zip Telepho	one #
State License # 3+3/42	License Class AS	City Busine	ess License # 99439	758-0351
Designer Name	Address	City	State/Zip Telephone	
State License # 465534				
8 WORKERS COMPENSATION Workers' Compensation Declaration: 1	pereby affirm under penalty of perior	y one of the following declaration	ALMA NI ANDERSKI DAŽBOLIČE. NS:	
	te of consent to self-insure for work			, for the performance
of the work for which this permit is issu	ed.			
I have and will maintain workers' issued. My worker's compensation insu	compensation, as required by Sect		r the performance of the work for □2;	which this permit is
Insurance Company Liberty	nutual		231654 - Expiration Date	12/01/04
(THIS SECTION NEED NOT BE COMPLE				' '
CERTIFICATE OF EXEMPTION: 1 of to become subject to the Workers' Com	certify that in the performance of the	work for which this permit is is:	sued, I shall not employ any persor	n in any manner so as
WARNING: Failure to secure workers'	compensation coverage is unlawful	l, and shall subject an employer	to criminal penalties and civil fine	es up to one hundred
thousand dollars (\$190,000), in addition	n to the cost of compensation, dama	- <i>I</i>	71/21/21	l attorney's fees.
SIGNATURE TUVE CARATION	Mully			
I hereby affirm that I am exempt from the	ne Contractor's License Law for the	following reason:		Harris, in an opportune to a contract preparation to compare to compare the contract of the co
I, as owner of the property or my (Sec. 7044, Business and Professions C				
such work himself or through his own e	mployees, provided that such improv	vements are not intended or offer	red for sale. If, however, the build	
sold within one year of completion, the	owner-builder will have the burden of exclusively contracting with licensed			ofessions Code: The
Contractor's License Law does not app	ply to an owner of property who b			
pursuant to the Contractor's License Law I am exempt under Section	w). Business and Professions	Code for this reason:		
-	jor labor and materials for constructi		rovement. TYES TNO	
	cation for a building permit for the pr			
3. I have contracted with the followi	ing person (firm) to provide the prop	oosed construction (include name	a / address / phone number / contr	actors license number):
4. I plan to provide portions of the we	ork, but I have hired the following p	erson to coordinate, supervise an	nd provide the major work (include	name / address / phone
number / contractors license number):				
I will provide some of the work, but of work):	ut I have contracted (hired) the folio	wing persons to provide the work	k indicated (include name / address	s / phone number / type
PROPERTY OWNER SIGNATURE		· · · · · · · · · · · · · · · · · · ·	DATE	
COMPLETE THIS SECTION FOR NON-RI	ESIDENTIAL BUILDING PERMITS ON			
is the applicant or future building occup	-			ement and prevention
program under Sections 25505, 25533	or 25534 of the Presley-Tanner Haz	rardous Substance Account Act?	YES NO	
Is the applicant or future building occupa		·	• •	YES NO
Is the facility to be constructed within 1	·	. – –		C LAPETING THE
IF ANY OF THE ANSWERS ARE YES, A REQUIREMENTS OF THE OFFICE OF EM	IERGENCY SERVICES AND THE AIR	POLLUTION CONTROL DISTRIC	эт.	·
8 CONSTRUCTION LENDING AGENC			AND THE REAL PROPERTY AND ADDRESS OF THE PARTY OF THE PAR	the state of the s
I hereby affirm that there is a construction			rmit is issued (Sec. 3097(i) Civil Co	ode).
LENDER'S NAME		ADDRESS		
I certify that I have read the application				
City ordinances and State laws relating property for inspection purposes. 1	to building construction. I hereby	authorize representatives of the	e City of Carlsbad to enter upon	the above mentioned
JUDGMENTS, COSTS AND EXPENSES				
OSHA: An OSHA permit is required for			•	16 AL - 15(1-2)
expiration: Every permit issued by the authorized by such permit is not commen				

APPLICANT'S SIGNATURE _



In Partnership with Government for Building Safety

DAT	E: August 24, 2004			☐ APPLICANT		
JURI	SDICTION: Carlsbad			☐ PLAN REVIEWER ☐ FILE		
PLAI	N CHECK NO.: 040907 R	Rev 1 (PCR0411	5) SET: III	u rice		
PRO	JECT ADDRESS: 6030 A	venida Encinas				
PRO	JECT NAME: STEEL CAN	IOPIES (Toyota	Carlsbad0			
\boxtimes	The plans transmitted hereventh with the jurisdiction's building		rected where necessa	ary and substantially comply		
	The plans transmitted herewhen minor deficiencies ide			isdiction's building codes by building department staff.		
	The plans transmitted here and should be corrected ar	_		ed on the enclosed check list		
	The check list transmitted herewith is for your information. The plans are being held at Esgil Corporation until corrected plans are submitted for recheck.					
	The applicant's copy of the contact person.	check list is enclose	sed for the jurisdiction	to forward to the applicant		
	The applicant's copy of the	check list has bee	n sent to:			
\boxtimes	Esgil Corporation staff did	not advise the app	olicant that the plan ch	eck has been completed.		
	Esgil Corporation staff did a Person contacted:	• •	nt that the plan check ephone #:	has been completed.		
	Date contacted: (Mail Telephone Fax REMARKS:	(by:) In Person	Fax #:			
	By: Abe Doliente Esgil Corporation GA MB EJ	En∉	closures:	trnsmti.dot		



In Partnership with Government for Building Safety

DAT	E: August 3, 2004			☐ APPLICANT ☑ JURIS. \		
JUR	ISDICTION: Carlsbad			☐ PLAN REVIEWER ☐ FILE		
PLA	N CHECK NO.: 040907 Rev 1 (PC)	R04115)	SET: II	■ FILE		
PRO	DJECT ADDRESS: 6030 Avenida E	ncinas				
PRO	DJECT NAME: STEEL CANOPIES					
	The plans transmitted herewith have to with the jurisdiction's building codes.	een corre	cted where necessa	ry and substantially comply		
	The plans transmitted herewith will su when minor deficiencies identified be	•	, ,	_		
	The plans transmitted herewith have and should be corrected and resubmit	_		ed on the enclosed check list		
\boxtimes	The check list transmitted herewith is for your information. The plans are being held at Esgil Corporation until corrected plans are submitted for recheck.					
	The applicant's copy of the check list contact person.	is enclose	d for the jurisdiction	to forward to the applicant		
\boxtimes	The applicant's copy of the check list Hamann Construction 1000 Pioneer Way, El Cajon, CA 920		sent to:			
	Esgil Corporation staff did not advise	the applic	ant that the plan che	eck has been completed.		
	Esgil Corporation staff did advise the Person contacted: Rebecca Date contacted: 4-04 (by: Par) Mail Telephone Fax In Person REMARKS:		Telephone #: 619/			
	By: Abe Doliente	Enclo	sures:			
	Esgil Corporation ☐ GA ☐ MB ☐ EJ ☐ PC	7/27/04		tmsmtl.dot		

Carlsbad 040907 Rev 1 (PCR04115) August 3, 2004

RECHECK PLAN CORRECTION LIST

JURISDICTION: Carlsbad

PLAN CHECK NO.: 040907 Rev 1

(PCR04115)

PROJECT ADDRESS: 6030 Avenida Encinas SET: II

DATE PLAN RECEIVED BY DATE RECHECK COMPLETED:

ESGIL CORPORATION: 7/27/04 August 3, 2004

REVIEWED BY: Abe Doliente

FOREWORD (PLEASE READ):

This plan review is limited to the technical requirements contained in the Uniform Building Code, Uniform Plumbing Code, Uniform Mechanical Code, National Electrical Code and state laws regulating energy conservation, noise attenuation and disabled access. This plan review is based on regulations enforced by the Building Department. You may have other corrections based on laws and ordinances enforced by the Planning Department, Engineering Department or other departments.

The following items listed need clarification, modification or change. All items must be satisfied before the plans will be in conformance with the cited codes and regulations. Per Sec. 106.4.3, 1997 Uniform Building Code, the approval of the plans does not permit the violation of any state, county or city law.

- A. Please make all corrections on the original tracings and submit two new sets of prints to: Esgil Corp. or to the bldg. dept. of the juris.
- B. To facilitate rechecking, please identify, next to each item, the sheet of the plans upon which each correction on this sheet has been made and return this sheet with the revised plans.
- C. The following items have not been resolved from the previous plan reviews. The original correction number has been given for your reference. In case you did not keep a copy of the prior correction list, we have enclosed those pages containing the outstanding corrections. Please contact me if you have any questions regarding these items.
- D. Please indicate here if any changes have been made to the plans that are not a result of corrections from this list. If there are other changes, please briefly describe them and where they are located on the plans. Have changes been made not resulting from this list?

. □Yes □No

Carlsbad 040907 Rev 1 (PCR04115) August 3, 2004

1. The addition of these steel canopies will affect the allowable area for building A. Revise the allowable area calculation. When a building has more than one occupancy, the area of the building shall be such that the sum of the rations of the actual area for each separate occupancy divided by the total allowable area for each separate occupancy shall not exceed one.

The jurisdiction has contracted with Esgil Corporation located at 9320 Chesapeake Drive, Suite 208, San Diego, California 92123; telephone number of 858/560-1468, to perform the plan review for your project. If you have any questions regarding these plan review items, please contact **Abe Doliente** at Esgil Corporation. Thank you.



In Partnership with Government for Building Safety

DAT	E: July 26, 2004			U APPLICANT U JURIS				
JUR	JURISDICTION: Carlsbad DELAN REVIEWER DEFILE							
PLA	N CHECK NO.: 040907 Rev 1 (PC)	R 04115) SE	Г: I	G FILE				
	DJECT ADDRESS: 6030 Avenida E	_						
PRC	DJECT NAME: STEEL CANOPIES	(TOYOTA	CARLSBAZ	>)				
	The plans transmitted herewith have be with the jurisdiction's building codes.	een corrected	where necessar	y and substantially comply				
	The plans transmitted herewith will sulwhen minor deficiencies identified bel	•						
	The plans transmitted herewith have s and should be corrected and resubmit	•		d on the enclosed check list				
\boxtimes	The check list transmitted herewith is for your information. The plans are being held at Esgil Corporation until corrected plans are submitted for recheck.							
	The applicant's copy of the check list i contact person.	s enclosed for	the jurisdiction t	to forward to the applicant				
\boxtimes	The applicant's copy of the check list I Hamann Construction 1000 Pioneer Way, El Cajon, CA 9202		to:					
	Esgil Corporation staff did not advise	the applicant tl	hat the plan che	ck has been completed.				
\boxtimes	Esgil Corporation staff did advise the Person contacted: Rebecca Date contacted: 7 26 04 (by: 6) Mail Felephone Fax In Person	• •	ephone #: 619/4	·				
	REMARKS:							
	By: Abe Doliente Esgil Corporation GA MB EJ PC	Enclosures	s:	trnsmtl.dot				

Carlsbad 040907 Rev 1 (PCR04115) July 26, 2004

GENERAL PLAN CORRECTION LIST

JURISDICTION: Carlsbad PLAN CHECK NO.: 040907 Rev 1

(PCR04115)

PROJECT ADDRESS: 6030 Avenida Encinas

DATE PLAN RECEIVED BY DATE REVIEW COMPLETED:

ESGIL CORPORATION: 7/15/04 **July 26, 2004**

REVIEWED BY: Abe Doliente

FOREWORD (PLEASE READ):

This plan review is limited to the technical requirements contained in the Uniform Building Code, Uniform Plumbing Code, Uniform Mechanical Code, National Electrical Code and state laws regulating energy conservation, noise attenuation and disabled access. This plan review is based on regulations enforced by the Building Department. You may have other corrections based on laws and ordinances enforced by the Planning Department, Engineering Department or other departments.

The following items listed need clarification, modification or change. All items must be satisfied before the plans will be in conformance with the cited codes and regulations. Per Sec. 106.4.3, 1997 Uniform Building Code, the approval of the plans does not permit the violation of any state, county or city law.

- Please make all corrections on the originals and submit three new *complete* sets of prints to: Esgil Corp. or to the bldg. dept. of the juris.
- To facilitate rechecking, please identify, next to each item, the sheet of the plans upon which each correction on this sheet has been made and return this sheet with the revised plans.
- Please indicate here if any changes have been made to the plans that are not a result of corrections from this list. If there are other changes, please briefly describe them and where they are located on the plans. Have changes been made not resulting from this list?

ם	Yes	No

Carlsbad 040907 Rev 1 (PCR04115) July 26, 2004

- 1. Provide a site plan showing the location of these two canopies. They must be clearly dimensioned from the property lines and from the existing adjacent buildings.
- 2. All sheets of the plans must be signed by the Architect or Engineer of record.
- 3. The jurisdiction has contracted with Esgil Corporation located at 9320 Chesapeake Drive, Suite 208, San Diego, California 92123; telephone number of 858/560-1468, to perform the plan review for your project. If you have any questions regarding these plan review items, please contact **Abe Doliente** at Esgil Corporation. Thank you.

Carlsbad 040907 Rev 1 (PCR04115) July 26, 2004

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VALUATION AND PLAN CHECK FEE

PLAN CHECK NO.: 040907 Rev 1 JURISDICTION: Carlsbad (PCR04115) PREPARED BY: Abe Doliente DATE: July 26, 2004 BUILDING ADDRESS: 6030 Avenida Encinas BUILDING OCCUPANCY: U-1 TYPE OF CONSTRUCTION: V-N BUILDING AREA VALUE Valuation Reg. (\$) PORTION Multiplier (Sq. Ft.) Mod. Canopy 1 1640 25.00 41,000 460 25.00 11,500 Canopy 2 Air Conditioning Fire Sprinklers 52,500 **TOTAL VALUE** Jurisdiction Code By Ordinance \$356.61 ₹. Bldg. Permit Fee by Ordinance \$231.80 Plan Check Fee by Ordinance \square Complete Review Type of Review: Structural Only ☐ Other __ Repetitive Fee Hour * Hourly

Esgil Plan Review Fee

Comments:

Repeats

Sheet 1 of 1 macvalue.doc

\$199.70



Sewer Fee Information Sheet

City of Carlsbad Public Works - Engineering

	BUILDING P	LANCHECK CHECKLIST
	_ du/s9	PLANCHECK NO .: CB 04 - 115
	TE: 8/9/07	renida Encinas
	OJECT DESCRIPTION: CW par	EST. VALUE:
AS	SESSOR'S PARCEL NUMBER:	EST. VALUE:
apprinter subrethis review conficare with susp	ENGINEERING APPROVAL item you have submitted for review has been roved. The approval is based on plans, rmation and/or specifications provided in your mittal; therefore any changes to these items after date, including field modifications, must be ewed by this office to insure continued formance with applicable codes. Please review efully all comments attached, as failure to comply instructions in this report can result in pension of permit to build. Right-of-Way permit is required prior to struction of the following improvements:	Please see the attached report of deficiencies marked with Make necessary corrections to plans or specifications for compliance with applicable codes and standards. Submit corrected plans and/or specifications to this office for review. By:
		By: Date:
		By: Date:
Ву:	ENGINEERING AUTHORIZATION	FOR OFFICIAL USE ONLY ON TO ISSUE BUILDING PERMIT: Date:
	ATTACHMENTS	ENGINEERING DEPT. CONTACT PERSON
	Dedication Application	Name: KATHLEEN M. FARMER
	Dedication Checklist	City of Carlsbad
	Improvement Application	Address: 1635 Faraday Avenue, Carlsbad, CA 92008
	Improvement Checklist	Phone: (760) 602-2741
	Future Improvement Agreement	CFD INFORMATION
	Grading Permit Application	Percel Man No.
	Grading Submittal Checklist	Lots:
	Right-of-Way Permit Application	Recordation:
	Right-of-Way Permit Submittal Checklist and Information Sheet	Carlsbad Tract:

	<u> SIT</u>	TE PLAN	
2 ND 3 RD	$\binom{1}{2}$	Provide a fully dimensioned site plant existing Structure North Arrow Existing & Proposed Structures Existing Street Improvements Property Lines Easements	lan drawn to scale. Show: Show Proposed Les. F. Right-of-Way Width & Adjacent Streets G. Driveway widths H. Existing or proposed sewer lateral I. Existing or proposed water service J. Existing or proposed irrigation service
	2.	Show on site plan:	
	D. 3.	percent towards an adjoining str 2. ADD THE FOLLOWING NOTE: drainage of 2% to swale 5' away Existing & Proposed Slopes and To Size, type, location, alignment of e (s) that serves the project. Each us second dwelling units and apartment Sewer and water laterals should no standards.	opography existing or proposed sewer and water service unit requires a separate service, however,
	В.	Site address Assessor's Parcel Number Legal Description	
		For commercial/industrial building total building square footage wit	gs and tenant improvement projects, include: th the square footage for each different use, quare footage of different uses (manufacturing, approved.
•		EXISTING PERMIT NUMBER	DESCRIPTION

1 ST	2 ND	3^{rd}	DISCRETIONARY APPROVAL COMPLIANCE
			4a. Project does not comply with the following Engineering Conditions of approval for Project No
			4b. All conditions are in compliance. Date:
. 4 \			DEDICATION REQUIREMENTS
M			 Dedication for all street Rights-of-Way adjacent to the building site and any storm drain or utility easements on the building site is required for all new buildings and for remodels with a value at or exceeding \$15,000, pursuant to Carlsbad Municipal Code Section 18.40.030.
			Dedication required as follows:
			Dedication required. Please have a registered Civil Engineer or Land Surveyor prepare the appropriate legal description together with an 8 ½" x 11" plat map and submit with a title report. All easement documents must be approved and signed by owner(s) prior to issuance of Building Permit. Attached please find an application form and submittal checklist for the dedication process. Submit the completed application form with the required checklist items and fees to the Engineering Department in person. Applications will not be accept by mail or fax.
			Dedication completed by: Date:
			IMPROVEMENT REQUIREMENTS
MA			6a. All needed public improvements upon and adjacent to the building site must be constructed at time of building construction whenever the value of the construction exceeds \$75,000, pursuant to Carlsbad Municipal Code Section 18.40.040.
			Public improvements required as follows:
			Attached please find an application form and submittal checklist for the public improvement requirements. A registered Civil Engineer must prepare the appropriate improvement plans and submit them together with the requirements on the attached checklist to the Engineering Department through a separate plan check process. The completed application form and the requirements on the

1 ST	2 ND	3 RD	checklist must be submitted in person. Applications by mail or fax are not accepted. Improvement plans must be approved, appropriate securities posted and fees paid prior to issuance of building permit.
			Improvement Plans signed by: Date:
			6b. Construction of the public improvements may be deferred pursuant to Carlsbad Municipal Code Section 18.40. Please submit a recent property title report or current grant deed on the property and processing fee of _\$310 _ so we may prepare the necessary Future Improvement Agreement. This agreement must be signed, notarized and approved by the City prior to issuance of a Building permit.
			Future public improvements required as follows:
			6c. Enclosed please find your Future Improvement Agreement. Please return agreement signed and notarized to the Engineering Department.
			Future Improvement Agreement completed by: Date:
			6d. No Public Improvements required. <u>SPECIAL NOTE: Damaged or defective improvements found adjacent to building site must be repaired to the satisfaction of the City Inspector prior to occupancy.</u>
			GRADING PERMIT REQUIREMENTS
. A			The conditions that invoke the need for a grading permit are found in Section 11.06.030 of the Municipal Code.
M			7a. Inadequate information available on Site Plan to make a determination on grading requirements. Include accurate grading quantities (cut, fill import, export).
A			7b. Grading Permit required. A separate grading plan prepared by a registered Civil Engineer must be submitted together with the completed application form attached. NOTE: The Grading Permit must be issued and rough grading approval obtained prior to issuance of a Building Permit.
			Grading Inspector sign off by: Date:
			7c. Graded Pad Certification required. (Note: Pad certification may be required even if a grading permit is not required.)

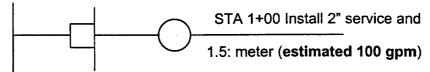
1 ^{s⊤}	2 ND □	3 RD	7d .No Grading Permit required.
			7e. If grading is not required, write "No Grading" on plot plan.
			MISCELLANEOUS PERMITS
			8. A RIGHT-OF-WAY PERMIT is required to do work in City Right-of-Way and/or private work adjacent to the public Right-of-Way. Types of work include, but are not limited to: street improvements, tree trimming, driveway construction, tying into public storm drain, sewer and water utilities.
			Right-of-Way permit required for:
			 INDUSTRIAL WASTE PERMIT If your facility is located in the City of Carlsbad sewer service area, you need to contact the Carlsbad Municipal Water District, located at 5950 El Camino Real, Carlsbad, CA 92008. District personnel can provide forms and assistance, and will check to see if your business enterprise is on the EWA Exempt List. You may telephone (760) 438-2722, extension 7153, for assistance.
			Industrial Waste permit accepted by:
_			Date:
			10. NPDES PERMIT Complies with the City's requirements of the National Pollutant Discharge Elimination System (NPDES) permit. The applicant shall provide best management practices to reduce surface pollutants to an acceptable level prior to discharge to sensitive areas. Plans for such improvements shall be approved by the City Engineer prior to issuance of grading or building permit, whichever occurs first.
Ø			11. Required fees are attached No fees required - Leld on Jugual Glds purmy WATER METER REVIEW
			 12a. Domestic (potable) Use Ensure that the meter proposed by the owner/developer is not oversized. Oversized meters are inaccurate during low-flow conditions. If it is oversized, for the life of the meter, the City will not accurately bill the owner for the water used. All single family dwelling units received "standard" 1" service with 5/8" service.

1ST 2ND 3RD

- If owner/developer proposes a size other than the "standard", then
 owner/developer must provide potable water demand calculations,
 which include total fixture counts and maximum water demand in gallons
 per minute (gpm). A typical fixture count and water demand worksheet is
 attached. Once the gpm is provided, check against the "meter sizing
 schedule" to verify the anticipated meter size for the unit.
- Maximum service and meter size is a 2" service with a 2" meter.
- If a developer is proposing a meter greater than 2", suggest the installation of multiple 2" services as needed to provide the anticipated demand. (manifolds are considered on case by case basis to limit multiple trenching into the street).
- 12b. Irrigation Use (where recycled water is **not** available)

All **irrigation meters** must be sized via irrigation calculations (in gpm) prior to approval. The developer must provide these calculations. Please follow these guidelines:

1. If the project is a newer development (newer than 1998), check the recent improvement plans and observe if the new irrigation service is reflected on the improvement sheets. If so, at the water meter station, the demand in gpm may be listed there. Irrigation services are listed with a circled "I", and potable water is typically a circled "W". The irrigation service should look like:



- 2. If the improvement plans do **not** list the irrigation meter and the service/meter will be installed via another instrument such as the building plans or grading plans (w/ a right of way permit of course), then the applicant must provide **irrigation calculations** for estimated worst-case irrigation demand (largest zone with the farthest reach). Typically, Larry Black has already reviewed this if landscape plans have been prepared, but the applicant must provide the calculations to you for your use. Once you have received a good example of irrigation calculations, keep a set for your reference. In general the calculations will include:
 - Hydraulic grade line
 - Elevation at point of connection (POC)
 - Pressure at POC in pounds per square inch (PSI)
 - Worse case zone (largest, farthest away from valve)
 - Total Sprinkler heads listed (with gpm use per head)
 - Include a 10% residual pressure at point of connection
- 3. In general, all major sloped areas of a subdivision/project are to be irrigated via separate irrigation meters (unless the project is only SFD with no HOA). As long as the project is located within the City recycled water

BUILDING PLANCHECK CHECKLIST 2ND 3RD 1ST service boundary, the City intends on switching these irrigation services/meters to a new recycled water line in the future. 12c. Irrigation Use (where recycled water is available) 1. Recycled water meters are sized the same as the irrigation meter above. 2. If a project fronts a street with recycled water, then they should be connecting to this line to irrigate slopes within the development. For subdivisions, this should have been identified, and implemented on the improvement plans. Installing recycled water meters is a benefit for the applicant since they are exempt from paying the San Diego County Water Capacity fees. However, if they front a street which the recycled water is there, but is not live (sometimes they are charged with potable water until recycled water is available), then the applicant must pay the San Diego Water Capacity Charge. If within three years, the recycled water line is charged with recycled water by CMWD, then the applicant can apply for a refund to the San Diego County Water Authority (SDCWA) for a refund. However, let the applicant know that we cannot guarantee the refund, and they must deal with the SDCWA for this. \sqcap 13. Additional Comments:

ENGINEERING DEPARTMENT FEE CALCULATION WORKSHEET

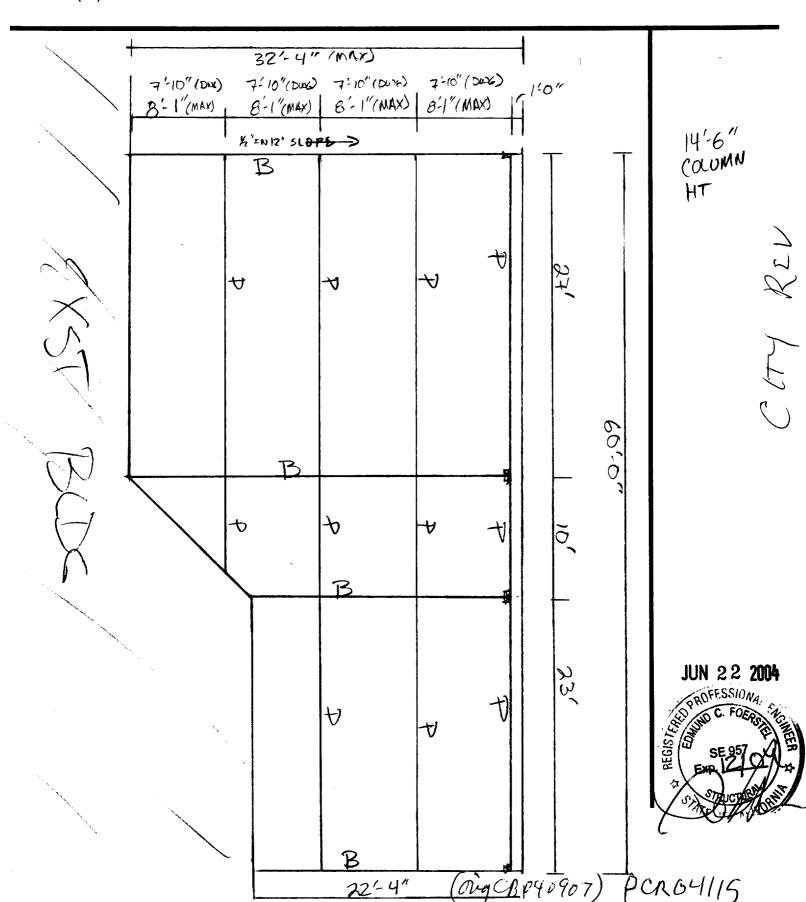
Αc	dress:			Bldg. Pe	ermit No	
	epared by:					
EC	OU CALCULATIONS:	List types and	d square f	ootages for all	uses.	
Ту	pes of Use:		Sq. Ft./Ui	nits:	EDU's: _	
Ту	pes of Use:		Sq. Ft./Ui	nits:	EDU's: _	
<u>A</u> [OT CALCULATIONS: L	ist types and	square fo	ootages for all	uses.	
Ту	pes of Use:		Sq. Ft./Ur	nits:	ADT's: _	
Ту	Types of Use:		Sq. Ft./Ur	nits:	ADT's:	
FE	ES REQUIRED:					
	ITHIN CFD: YES (no	bridge & thord	ughfare fe	e in District #1, i	reduced Traffic Impa	ct Fee) 🗀 NO
	1 DADE MILIEU EEE	DARK	ADEA 0. #.		·	
ט	1. PARK-IN-LIEU FEE FEE/UNIT:	•			= \$	
	2. TRAFFIC IMPACT FE		^	NO. UNITS		
_			×	FEE/ADT:	= \$	
	3. BRIDGE AND THORO					
					 = \$	
	4. FACILITIES MANAGE					
	UNIT/SQ.FT	·:	×	FEE/SQ.FT./UN	NIT: = \$	
	5. SEWER FEE					
	EDU's:		x	FEE/EDU:	= \$	
	BENEFIT AREA:	<u>.</u>				
	EDU's:		X	FEE/EDU:	= \$	
	6. SEWER LATERAL (\$	2,500)	•		= \$	
	7. DRAINAGE FEES	PLDA	:	HIGH	_ /LOW	
	ACRES:	***	X	FEE/AC:	= \$	
	8. POTABLE WATER F	EES				
	LINITE CODE	CONNECTION	CCC	METER FEE	SDCWA FEE	IRRIGATION

PLANNING DEPARTMENT
BUILDING PLAN CHECK REVIEW CHECKLIST

10/1	Plan Check No. CB PCROHIS Address 6030 AVd. ENCWA
A Com	Planner Greg Fisher Phone (760) 602- 4629
100	APN:
Date Date	Type of Project & Use: Net Project Density: DU/AC
$M_{M_{\perp}}$	Zoning: M General Plan: PI Facilities Management Zone:
THE STATE OF THE S	CFD (in/out) #_Date of participation: Remaining net dev acres:
Plan Check #1 by Plan Check #2 by Plan Check #3 by	Circle One (For non-residential development: Type of land used created by this permit:)
Plan Plan	Legend:
$\Delta \Box \Box$	Environmental Review Required: YES NO TYPE
	DATE OF COMPLETION:
1	Compliance with conditions of approval? If not, state conditions which require action. Conditions of Approval:
\Box	Discretionary Action Required: YES NO TYPE
٢	APPROVAL/RESO. NO DATE
	PROJECT NO
\	OTHER RELATED CASES:
	Compliance with conditions or approval? If not, state conditions which require action. Conditions of Approval:
	Coastal Zone Assessment/Compliance
	Project site located in Coastal Zone? YES NO
	CA Coastal Commission Authority? YESNO If California Coastal Commission Authority: Contact them at - 7575 Metropolitan Drive, Suite 103, San Diego CA 92108-4402; (619) 767-2370
	Determine status (Coastal Permit Required or Exempt):
•	Coastal Permit Determination Form already completed? YES NO If NO, complete Coastal Permit Determination Form now.
	Coastal Permit Determination Log #:
	Follow-Up Actions:
	 Stamp Building Plans as "Exempt" or "Coastal Permit Required" (at minimum Floor Plans). Complete Coastal Permit Determination Log as needed.
	Inclusionary Housing Fee required: YES NO (Effective date of Inclusionary Housing Ordinance - May 21, 1993.)
	Data Entry Completed? YES NO (A/P/Ds, Activity Maintenance, enter CB#, toolbar, Screens, Housing Fees, Construct Housing Y/N, Enter Fee, UPDATE!)

\sim \wedge	Site Plan:		
	easements, existing ar	nd proposed structur	n to scale. Show: North arrow, property lines res, streets, existing street improvements, right xisting topographical lines (including all side an
	2. Provide legal descriptio	n of property and as	sessor's parcel number.
^	Policy 44 - Neighborhood	Architectural Desig	n Guidelines
K(I) 🗆 🗆	1. Applicability: YES	NO	
	2. Project complies YES_		
(Zoning:		
	1. Setbacks:		
	Front:	Required	Shown
	Interior Side:	Required	
	Street Side:	Required	Shown
	Rear:		Shown
	Top of slope:	Required	
	2. Accessory structure se	tbacks:	
	Front:	Required	Shown
	Interior Side:	Required	Shown
	Street Side:	Required	
	Rear:	Required	
	Structure separation:	Required	
	3. Lot Coverage:	Required	Shown
	4. Height:	Required	Shown
	-	s Required	
		•	ial and industrial projects required)
4	Residential Guest Spaces R	equired	Shown
	Additional Comments	Jegg Pio	vide A telly
			
4.	DIMENSILWAR ?	site plan	I DRAWN TO SCALE.
	SHOW DODOSER	+ EXISTIN	a structures with
	- HOW FIVE		
	Cet BANS.		, ,
	50,000		9/31/04
OK TO ISSUE	AND ENTERED APPROVAL IN	TO COMPUTER	DATE

SHEET:<u>1</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>



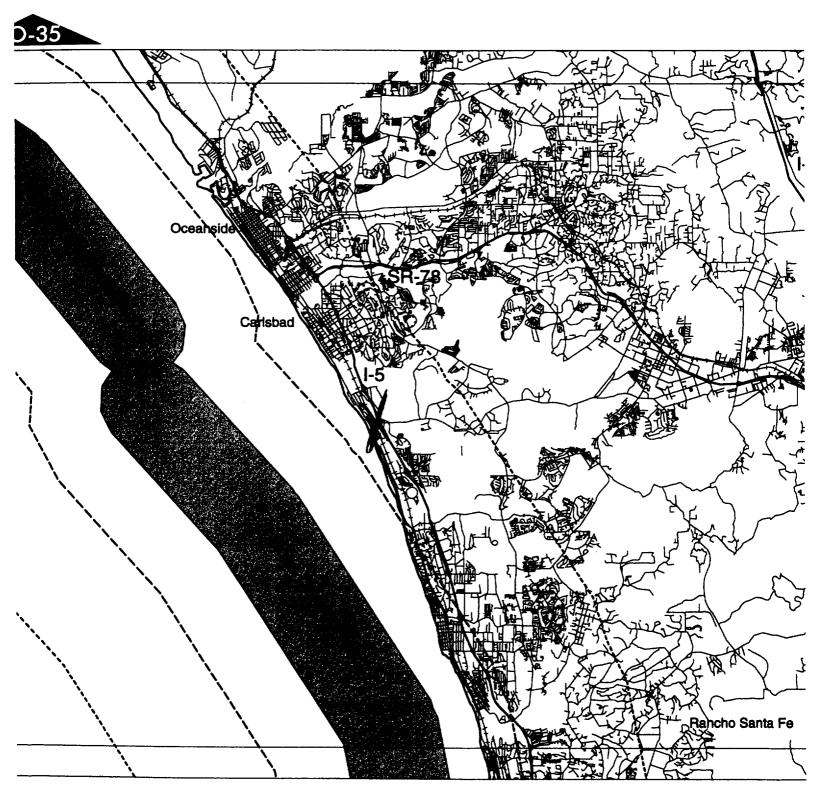
10km2P-Faul+ 25 km

Na=1.0

1-36

Nv = 1.2 Active Fault Near-Source Zon This map is intended to be used in conjunction with

the 1997 Uniform Building Code, Tables 16-S and 16-T



****	A A						
****		N		AE'	57		-
-	191		X *			*	-

Send To Printer Back to Map

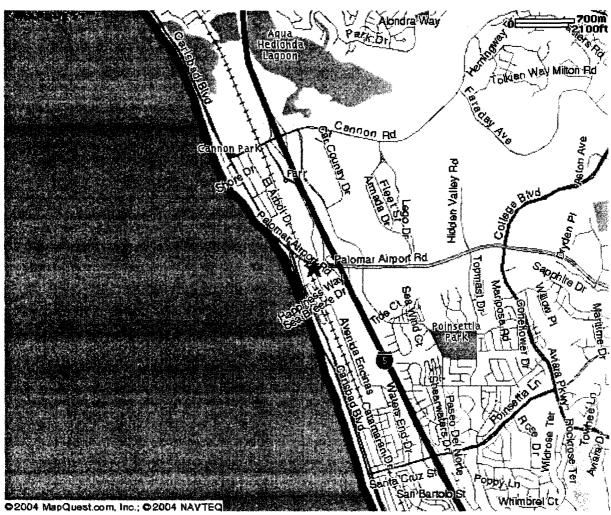
6030 Avenida Encinas Carlsbad CA 92009-1061 US

Notes:	

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NAVTEO ON EGAID



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TABLE 3-CARBON STEEL KWIK BOLT-II ALLOWABLE TENSION AND SHEAR VALUES (In pounds), NORMAL-WEIGHT CONCRETE^{1,2}

	T	T T	&" = 2,000 pel			&" = 2,000 pel		T	6' = 4,000 pel			£" - 0,000 pel	
	AMCMOR	Tee	alen		7	alea		Timeles			The state of the s	elan i	
ANCHOR DIAMETIM Goods	DEPTH	Typ. lasg.	Ythou Sp. lasp.		Sp. Inop.	Without Sp. leep.	Sheer	NAME OF THE PARTY	St. Insp.	Steer	gir justi 1980	Without Sp. loop.	Steer
	11/83	245	120	400	300	150	400	350	175	400	430	215	400
1/4	2	525	265	400	550	290	400	590	295	400	625	315	400
]	33/4	625	315	400	625	315	400	625	315	400	625	315	400
	15/83	500	250	925	605	300	975	710	355	1,025	800	400	1,025
3/2	21/2	1,125	565	1,100	1,210	605	1,100	1,290	645	1,100	1,450	725	1,100
ĺ	41/4	1,190	595	1,100	1,235	615	1,100	1,285	640	1,100	1,450	725	1,100
	21/43	860	430	1,810	960	490	1,840	1,065	530	1,840	1,625	815	1,340
1/2	31/2	1,750	875	1,840	2,000	1,000	1,840	2,250	1,125	1,840	2,625	1,315	1,840
·	6	1,950	975	1,840	2,165	1,080	1,840	2,375	1,190	L,840	2,625	1,315	1,840*
	23/43	1,425	710	2,875	1,685	845	2,875	1,950	975	2,875	2,500	1,250	2,875
5/8	4	2,180	1,125	3,125	2,670	1,335	3,125	3,090	1,545	3,125	3,925	1,965	3,125
	7	3,000	1,500	3,125	3,250	1,625	3,125	3,500	1,750	3,125	3,925	1,965	3,125
	31/43	1,850	925	3,875	2,175	1,090	3,875	2,500	1,250	3,875	3,000	1,500	3,875
3/4	43/4	2,750	1,375	4,225	3,625	1,940	4,225	4,500	2,250	4,225	5,060	2,530	4,225
	8	3,750	1,875	4,225	4,625	2,315	4,225	5,500	2,750	4,225	5,925	2,965	4,225
	41/23	2,930	1,465	6,625	3,650	1,825	7,125	4,375	2,190	7,625	4,360	2,180	8,625
1	6	3,990	1,995	8,625	5,310	2,655	8,625	6,625	3,315	8,625	7,875	3,940	8,625
	9	6,040	3,020	8,625	7,050	3,525	8,625	8,055	4,025	8,625	10,000	5,000	8,625

For SE: 1 inch = 25.4 mm, 1 psi = 6.9 kPa, 1 lb. = 4.45 N.

TABLE 4—STAINLESS STEEL KWIK BOLT-II ALLOWABLE TENSION AND SHEAR VALUES (In pounds), NORMAL-WEIGHT CONCRETE^{1,2}

	[T	6' + 2,500 pel.		T	6' = 2,000 pel			\$" = 4,000 pel			§' = 8,000 pel	
ANCHOR	ANCHOR	ANCHOR Transfer		T	700	Transfers		* Benefes) he	Jean .	
PARCHOR PARETIES ARCHOR	DEPTH	Nya. Sp. insp.	Sp. imp.	Sheer	Sår jandr 1880	Millered Sp. Imp	-	NAS. Sp. Imap.	Sp. leep.	Short	Sp. leep.	Sp. loop. Without	Sheer
	13/83	170	85	525	230	115	540	245	120	550	350	175	550
1/4	2	425	210	550	500	250	550	500	250	550	520	260	550
	33/4	520	260	550	520	260	550	520	260	550	520	260	550
	15/83	400	200	825	460	230	950	515	260	1,075	625	315	1,150
3/2	21/2	875	440	1,250	1,025	515	1,250	1,175	590	1,250	1,350	675	1,250
•	41/4	1,000	500	1,250	1,145	625	1,250	1,350	675	1,250	1,350	675	1,250
	21/43	800	400	1,700	1,000	500	1,740	1,200	600	1,775	1,250	625∙	2,085
1/2	31/2	1,250	625	2,085	1,625	\$15 1	2,085	2,000	1,000	2,085	2,250	1,125	2,085 ·
	6	1,375	690	2,085	1,765	880	2,085	2,150	1,075	2,085	2,550	1,275	2,065
	23/43	1,020	510	2,625	1,250	625 ·	2,875	1,475	735	3,125	1,800	900	3,125
5/8	4	1,730	\$65	3,125	2,220	1,110	3,125	2,715	1,355	3,125	3,000	1,500	3,125
	7	2,250	1,125	3,125	2,825	1,415	3,125	3,425	1,715	3,125	3,425	1,715	3,125
	31/43	1,450	725	2,700	1,825	915	3,100	2,200	1,100	3,500	2,450	1,225	4,500
3/4	43/4	2,350	1,175	4,225	2,990	1,495	4,365	3,625	1,815	4,500	4,375	2,190	4,500
	8	2,750	1,375	4,500	3,500	1,815	4,500	4,250	2,125	4,500	4,800	2,400	4,500
	41/23	2,300	1,150	5,700	2,850	1,425	6,350	3,400	1,700	7,000	4,500	2,250	7,000
1	6	3,740	1,870	7,000	4,930	2,465	7,000	6,120	3,060	7,000	6,875	3,440	7,000
	9	5,250	2,625	7,000	7,075	3,540	7,000	8,890	4,400	7,000	8,800	4,400	7,000

For SI: 1 inch = 25.4 mm, 1 pri = 6.9 kPa, 1 lb. = 4.45 N.

¹See Table 2 footnotes.

²Allowable loads may be increased by 33½ percent for short-term loading due to wind or seismic forces.

Only the long-threaded style KB-II anchor installed at this embedment depth is permitted to be used to resist shear due to wind or seismic forces. Long threaded style KB-II anchors have a thread length greater than three bolt diameters.

¹See Table 2 footnotes.

²Allowable loads may be increased by 33½, percent for short-term loading due to wind or seismic forces.

³Anohors installed at this embedment depth shall not be used to resist shear due to wind or seismic forces.

M-C TOYOTA OF CARLSBAD

SHEET:<u>2</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

Dead Loads						
Roof Deck	1.00	psf				
Purlins	1.50	psf				.]
Beam	1.50	psf	_			ı
Total	4.00	psf				
Decking						DECKING
						HR-36 AEP 26 GAUGE
SIMPLE SPAN						GAUGE
Trib. Width (TW) =	1.00	ft	Dead Load (DL) =	1.00	psf	
Length (L) =	7.83	ft	Live Load (LL) =	20.00	psf	
F _b =	50,000.00	psi	Total Load (TL) =	21.00	psf	
w = TL*TW =	21.00	plf				
$M = (w^*L^2)/8 =$	161.07	ft-lb				
$S_{req} = M/F_b =$	0.0387	in³/ft				
Use HR-36 AEP 26	gauge	S=	0.0895	in³/ft	ОК	
CANTILEVER SPAN						
Trib. Width (TW) =	1.00	ft	Dead Load (DL) =	1.00	psf	
Length (L) =	1.00	ft	Live Load (LL) =	20.00	psf	
Fb	50,000.00	psi	Total Load (TL) =	21.00	psf	
w = TL*TW =	21.00	plf				
M= (w*L²)2 =	10.50	ft-lb				
$S_{req} = M/F_b =$	0.0025	in ³ /ft	SIMPLE SPAN GOVE	ERNS		
<u>PURLINS</u>						<u>PURLINS</u>
						10 C 12 X 3.25 AEP
Trib. Width (TW) =	8.08	ft	Dead Load (DL) =	2.50	psf	OR 12 C 14 X 4
Length (L) =	27.00	ft	Live Load (LL) =	16.00	psf	POWERS
Trib. Area (TA) =	218.25	ft ²	Total Load (TL) =	18.50	psf	1
F _b	30,000.00	psi			L	
w = TL*TW =	149.54	plf				

M-C TOYOTA OF CARLSBAD

SHEET:<u>3</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6</u>/8/2004BY:<u>DKR</u>

DUDI INC						
PURLINS			•			
$V_L=V_R=(w^*L)/2=$	2,018.81	lb				
$M = (w^*L^2)/8 =$	13,626.98	ft-lb				
S _{req} = M/F _b =	5.4508	in ³				
Use 10C12X3.25 AB OR	ΕP	S=	5.5270	in ³	ОК	
Use 12C14X4 POW	ERS	S=	5.5470	in ³	ОК	
<u>BEAM</u>						BEAM
<u>SEAM</u>						2 - 17 C 12 X 3 AEP
Trib. Width (TW) □	18.50	ft	Dead Load (DL) =	4.00	psf	OR 2 - 16 C 12 X 4
Length (L) =	32.33	ft	Live Load (LL) =	16.00	psf	POWERS
Trib. Area (TA) =	598.17	ft ²	Total Load (TL) =	20.00	psf	OR
F _b =	30,000.00	psi				2 - 12 C 10 X 4 POWERS
w = TL*TW =	370.00	plf				
V_L OR V_R = (w*L)/2 =	5,981.67	lb				
$M = (w^*L^2)/8 =$	48,351.81	ft-lb				
$S_{req} = M/F_b =$	19.3407	in ³				
USING 2 SECTIONS						
$S_{req-FOR 2} = (M/F_b)/2 =$	9.6704	in ³				
Use 2-17C12X3 AE OR	Р	S=	9.6870	in ³	ОК	
Use 2-16C12X4 PC OR	WERS	S=	11.7000	in ³	OK	
Use 2-12C10X4 PC	WERS	S=	10.1200	in ³	ОК	

M-C TOYOTA OF CARLSBAD

SHEET:<u>4</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

COL	UMN				<u>-</u>		COLUMN
	VERTICAL LOADS						2 - 10 C 12 X 3.25 AEP WELDED TOGETHER
	Trib. Width (TW) =	18.50	ft	Dead Load (DL) =	4.00	psf	
	Length (L) =	16.17	ft	Live Load (LL) =	16.00	psf	
	Trib. Area (TA) =	299.08	ft ²	Total Load (TL) =	20.00	psf	
	F _y =	55,000.00	psi	F _b =	30,000.00	psi	
	Total Dead Load (T	'DL) =	DL*TA				
	TDL =	1,196.33	lb				
	Total Live Load (TL		LL*TA				
	TLL =	4,785.33	lb				
	Total Vertical Load	(TVL) =	TDL+TLL				
	TVL =	5,981.67	lb				
	WIND LOAD	70 MPH EXP	. C				
	P =	$q_s{}^*C_eC_qI_w$					
		$q_s =$	12.60				
		C _e =	1.06				
		C ^d =	1.30	horizontal	0.70	upward	
		I _w =	1.00				
	P _H =	17.36	psf				
	P _U =	9.35	psf				
	HEICHT OF BOOK	· // N =	CLODE *	I ENGTHER			
	HEIGHT OF ROOF SLOPE	· (n) = 1/24	SLOPE "	LENGTH (L) 32.33	ft		
	SLOPE	1/24	L -	32.33	11,		
	H =	1.35	ft				
	Trib. Width (TW) =	18.50	ft	Dead Load (DL) =	4.00	psf	
	Trib. Length (L) =	16.17	ft	Live Load (LL) =	16.00	psf	
	Trib. Area (TA) =	299.08	ft²	Total Load (TL) □	20.00	psf	
	F _b =	22,000.00	psi	COLUMN HT (CH) =	14.50	ft	
	NUMBER OF COL	UMNS (n) =	2.00				
	WIND FORCE (W))=	P _H *H*TW/	n			
	W =	216.37	lb				

M-C TOYOTA OF CARLSBAD

SHEET:<u>5</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

COLUMN					
SEISMIC LOAD					
ZONE =	4.00		DESIGN BASE SHEAF	₹	
C _a =	0.44		$V = (C_v^*I^*W)/(R^*T) =$	2.20	*W
C _v =	0.77		V =	2,629.03	lb
R =	2.20				
1 =	1.00		MAX DESIGN SHEAR		
h _n =	15.85		$V = (2.5 C_a^*I^*W)/(R) =$	0.50	*W
$C_t =$	0.02		V =	598.17	lb
T =	0.16				
N _a =	1.00	MIN	NE 4)		
$N_v =$	1.20	,	$V = (.8*Z*N_v*I*W)/(R) =$	0.17	*W
Z =	0.40		V =	208.81	lb
Soil Profile Type =	S₀				
Seismic Source =	В				
Distance To Source =	≥ 5 km				
Trib. Width (TW) =	18.50	ft	Dead Load (DL) =	4.00	psf
Length (L) =	16.17	ft	Live Load (LL) =	16.00	psf
Trib. Area (TA) =	299.08	ft²	Total Load (TL) =	20.00	psf
			COLUMN HT (CH) =	14.50	ft
W =	DL*TA				
w =	1,196.33	lb			
	.,				
$V_{TOTAL} =$	3,320.00	lb	A _B =	1,660.00	ft ²
r _{max} =	V/V _{TOTAL}				
r _{max} =	0.18				
ρ = 2	2-((20)/(r _{max} *sq	rt(A _B)))			
ρ =	1.00				
E =	ρ *V				
E =	598.17	lb			
E/1.4 =	427.26	lb			

M-C TOYOTA OF CARLSBAD

SHEET:<u>6</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

STRUCTURAL ENGINEER 1046 CALLE RECODO SUITE J SAN CLEMENTE, CA 92673 PHONE (949)492-5981 FAX (949)498-3020

COLUMN

<u>.UMN</u>									
STRONG DIRECTIO	<u>N</u>								
LOAD CASE 1 D									
D = LOAD CASE 2 D + L	TDL		DOES NOT GOVE	RN LESS THAN	LOAD CASE 2				
D + L = <u>LOAD CASE 3</u> D+(W or E/1.4)	TVL								
D+(W or E/1.4) = <u>LOAD CASE 4</u> .9D +/- E/1.4	D + E/1.4								
	.9D +/- E/1.5 = .9D +/- E/1.4 DOES NOT GOVERN LESS THAN LOAD CASE 3								
D + .75*[L+(W or E D + .75*[L+(W or E		D + .75*	L + .75*(E/1.4)						
TRY 2 - 10 C 12 X	3.25 AEP								
	2.59	in ²							
S _x =	11.05	in ^a	S _y =	2.38	in ³				
r _x =	7.71	in	r _y =	2.41	in				
COLUMN HT (I) =		ft	K =	2.10					
LOAD CASE 2									
D+L=	TVL								
D + L =	5,981.67	lb							
M =	NONE			•					
M =	0.00	ft-lb							
f _a =	TVL/A		f _b =	M/S					
f _a =	2,311.31	psi	f _b =	0.00					
KI/r =	47.38								
F _a =	24,752.89	psi	F _b =	30,000.00	psi				
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.00 0.09 0.09	OK OK							

M-C TOYOTA OF CARLSBAD

SHEET:70F:42 JOB NO:04D141 DATE:6/8/2004BY:DKR

STRUCTURAL ENGINEER 1046 CALLE RECODO SUITE J SAN CLEMENTE, CA 92673 PHONE (949)492-5981 FAX (949)498-3020

COLUMN

STRONG DIRECTION

LOAD CASE 3	GOVERNS				
D+(W or E/1.4) =	D + E/1.4				
D =	TDL				
D =	1,196 .33	lb	VERTICAL LOAD		
E/1.4 =	427.26	lb	HORIZONTAL LOAI	D	
M =	(E/1.4)*I				
M =	6,195.30	ft-ib			
f _e =	TDL/A		f _b =	M/S	
f _a =	462.26	psi	f _b =	6,725.49	psi
KI/r =	47.38				
F _e =	24,752.89	psi	F _b =	30,000.00	psi
fa/Fa +/- fb/Fb ≤	1.33		LATERAL		
fa/Fa + fb/Fb =	0.2429	OK	LATERAL		
			LATERAL		
fa/Fa + fb/Fb =	0.2429	OK	LATERAL		
fa/Fa + fb/Fb = fa/Fa - fb/Fb =	0.2429 -0.21	OK OK			
fa/Fa + fb/Fb = fa/Fa - fb/Fb = LOAD CASE 5 D + .75*[L+(W or E	0.2429 -0.21 E/1.4)] = TDL	OK OK D+.75*			
fa/Fa + fb/Fb = fa/Fa - fb/Fb = LOAD CASE 5 D + .75*[L+(W or E	0.2429 -0.21 E/1.4)] =	OK OK			
fa/Fa + fb/Fb = fa/Fa - fb/Fb = LOAD CASE 5 D + .75*[L+(W or E D = D = .75*L =	0.2429 -0.21 E/1.4)] = TDL	OK OK D+.75*			
fa/Fa + fb/Fb = fa/Fa - fb/Fb = LOAD CASE 5 D + .75*[L+(W or E D = D =	0.2429 -0.21 E/1.4)] = TDL 1,196.33	OK OK D+.75*			
fa/Fa + fb/Fb = fa/Fa - fb/Fb = LOAD CASE 5 D + .75*[L+(W or E D = D = .75*L =	0.2429 -0.21 = [/1.4)] = TDL 1,196.33	OK OK D + .75*			
fa/Fa + fb/Fb = fa/Fa - fb/Fb = LOAD CASE 5 D + .75*[L+(W or E D = D = .75*L = .75*L =	0.2429 -0.21 = (1.4)] = TDL 1,196.33 .75*TLL 3,589.00	OK OK D + .75*			
fa/Fa + fb/Fb = fa/Fa - fb/Fb = LOAD CASE 5 D + .75*[L+(W or E D = D = .75*L = .75*L = VL = VL = VL = .75*(E/1.4) =	0.2429 -0.21 = TDL 1,196.33 .75*TLL 3,589.00 D+.75*L 4,785.33	OK OK D + .75* Ib			

(.75*(E/1.4))*I

4,646.47

ft-lb

M =

M =

M-C TOYOTA OF CARLSBAD

SHEET:<u>8</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:6/8/2004BY:DKR

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2				N.I
ÇO	ᆫ	U	M	N

STRONG DIRECTION

LOAD CASE 5

 $f_a = VL/A$ $f_b = M/S$ $f_a = 1,849.05$ psi $f_b = 5,044.12$ psi

KI/r = 47.38

 $F_a = 24,752.89$ psi $F_b = 30,000.00$ psi

fa/Fa +/- fb/Fb ≤ 1.33 DUE TO LATERAL

fa/Fa + fb/Fb = 0.2428 OK fa/Fa - fb/Fb = -0.09 OK

WEAK DIRECTION

LOAD CASE 1

D = TDL DOES NOT GOVERN LESS THAN LOAD CASE 2

LOAD CASE 2

D+L

D + L = TVL

LOAD CASE 3

D+(W or E/1.4)

D+(W or E/1.4) = D + E/1.4

LOAD CASE 4

.9D +/- E/1.4

.9D +/- E/1.5 = .9D +/- E/1.4 DOES NOT GOVERN LESS THAN LOAD CASE 3

LOAD CASE 5

D + .75*[L+(W or E/1.4)]

D + .75*[L+(W or E/1.4)] = D + .75*L + .75*(E/1.4)

14.50

TRY 2 - 10 C 12 X 3.25 AEP

 $A = 2.59 in^2$ $S_x = 11.05 in^3 S_y = 2.38 in^3$ $r_x = 7.71 in r_y = 2.41 in$

ft

K =

2.10

COLUMN HT (I) = LOAD CASE 2

D + L = TVL D + L = 5,981.67 lb

M-C TOYOTA OF CARLSBAD

SHEET:<u>9</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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COLUMN

WEAK DIRECTION

LOAD CASE 2

M = M =	NONE 0.00	ft-lb			
f _a =	TVL/A		f _b =	M/S	
f _a =	2,311.31	psi	f _b =	0.00	
- u	2,011.01	poi	-р	0.00	
KI/r =	151.87				
F _a =	6,471.67	psi	F _b =	30,000.00	psi
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.00 0.36 0.36	OK OK			
LOAD CASE 3	GOVERNS				
D+(W or E/1.4) =	D + E/1.4				
D =	TDL				
D =	1,196.33	lb	VERTICAL LOAD		
E/1.4 =	427.26	lb	HORIZONTAL LOAL)	
M =	(E/1.4)*I				
M =	6,195.30	ft-lb			
. =			£		
f _a ⊟	TDL/A		f _b =	M/S	
f _a =	462.26	psi	f _b =	31,210.57	psi
KI/r =	151.87				
F _a =	6,471.67	psi	F _b =	30,000.00	psi
fa/Fa +/- fb/Fb ≤	1.33	DUE TO	LATERAL		
fa/Fa + fb/Fb =	1.11	OK			
fa/Fa - fb/Fb =	-0.97	ОК			
LOAD CASE S					
LOAD CASE 5 D + .75*[L+(W or	F/1 4)] =	D + 75*	L + .75*(E/1.4)		
= (2. (4. 0)	~ ··¬/J	J 0	(_,,		

M-C TOYOTA OF CARLSBAD

SHEET:<u>10</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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\sim			8.5	M
CO	ᆫ	u	M	N

WEAK DIRECTION

LOAD CASE 5

fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.33 1.07 -0.49	DUE TO OK OK	LATERAL		
F _a =	6,471.67	psi	F _b =	30,000.00	psi
KI/r =	151.87				
f _a =	1,849.05	psi	$f_b =$	23,407.93	psi
f _a =	VL/A		f _b =	M/S	
M = M =	(.75*(E/1.4))*I 4,646.47	ft-lb			
.75*(E/1.4) =	320.45	lb			
.75*(E/1.4) =	.75*(E/1.4)				
VL =	4,785.33	lb			
VL =	D+.75*L				
.75*L = .75*L =	.75*TLL 3,589.00	lb			
	-	10			
D = D =	TDL 1,196.33	lb			

M-C TOYOTA OF CARLSBAD

SHEET:<u>11</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

COLUMN						ALT. CO
VERTICAL LOADS						1133 0 %
Trib. Width (TW) =	18.50	ft	Dead Load (DL) =	4.00	psf	
Length (L) =	16.17	ft	Live Load (LL) =	16.00	psf	
Trib. Area (TA) =	299.08	ft ²	Total Load (TL) =	20.00	psf	
F _y =	46,000.00	psi	F _b □	22,000.00	psi	
Total Dead Load (T	DL) =	DL*TA				
TDL =	1,196.33	lb				
Total Live Load (TL		LL*TA				
TLL =	4,785.33	lb				
Total Vertical Load		TDL+TLL				
TVL =	5,981.67	lb				
WIND LOAD	70 MPH EXP.	C				
P =	$q_s^*C_e^C_q^l_w$					
	$q_s =$	12.60				
	C _e =	1.06				İ
	C ^d =	1.30	horizontal	0.70	upward	
	I _w =	1.00			·	
P _H =	17.36	psf				
P _U =	9.35	psf				
HEIGHT OF ROOF	: (H) =	SLOPE *	LENGTH (L)			1
SLOPE	1/24	L =	32.33	ft		
H =	1.35	ft				
Trib. Width (TW) =	18.50	ft	Dead Load (DL) =	4.00	psf	
Trib. Length (L) =	16.17	ft	Live Load (LL) =	16.00	psf	
Trib. Area (TA) =	299.08	ft²	Total Load (TL) =	20.00	psf	
F _b =	22,000.00	psi	COLUMN HT (CH) =	14.50	ft	
NUMBER OF COL	UMNS (n) =	2.00				
WIND FORCE (W)	=	P _H *H*TW/i	1			
W =	216.37	lb				1

M-C TOYOTA OF CARLSBAD

SHEET:<u>12</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

ET. OOLOMIN					
SEISMIC LOAD			-		
ZONE =	4.00		DESIGN BASE SHEAR		
C _a =	0.44		$V = (C_v^*I^*W)/(R^*T) =$	2.20	*W
C, =	0.77		V =	2,629.03	lb
R=	2.20			_,	
! =	1.00		MAX DESIGN SHEAR		
h _n =	15.85		$V = (2.5 C_a^* I^* W)/(R) =$	0.50	*W
$C_t =$	0.02		V =	598.17	lb
T =	0.16				
N _a =	1.00	Mil	N DESIGN SHEAR (ZON	IE 4)	
N _v =	1.20		$V = (.8*Z*N_v*I*W)/(R) =$	0.17	*W
Z =	0.40		V =	208.81	lb
Soil Profile Type	S _d				
Seismic Source =	В				
Distance To Source =	≥ 5 km				
Trib. Width (TW) =	18.50	ft	Dead Load (DL) =	4.00	nof
Length (L) =	16.17	ft	Live Load (LL) =	16.00	psf psf
Trib. Area (TA) =	299.08	ft ²	Total Load (TL) =	20.00	psf
F _b =	22,000.00	psi	COLUMN HT (CH) =	14.50	ft
2	•	•	,		
W =	DL*TA				
W =	1,196.33	lb			
V _{TOTAL} =	3,320.00	lb	A _B =	1,660.00	ft²
r _{mex} =	V/V _{TOTAL}				
r _{mex} =	0.18				
ρ = 2	2-((20)/(r _{max} *so	qrt(A _B)))			
ρ =	1.00				
E =	$ ho^{ullet}$				
E = E/1.4 =	598.17 427.2 6	lb lb			

M-C TOYOTA OF CARLSBAD

SHEET:<u>13</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

STRONG DIRECTION

STRONG DIRECTIC	<u> N</u>				
LOAD CASE 1					
D					
D =	TDL		DOES NOT GOVE	ERN LESS THAN	LOAD CASE 2
LOAD CASE 2					
D+L					
D + L =	TVL				
LOAD CASE 3					
D+(W or E/1.4)					
D+(W or E/1.4) =	D + E/1.4				
LOAD CASE 4					
.9D +/- E/1.4					
.9D +/- E/1.5 =	.9D +/- E/1.4		DOES NOT GOVE	ERN LESS THAN	LOAD CASE 3
LOAD CASE 5					
D + .75*[L+(W or 8	∃/1.4)]				
D + .75*[L+(W or 8	E/1.4)] =	D + .75*	L + .75*(E/1.4)		
TRY A HSS 6 X 6	X 1/8				
A =	2.70	in ²			
S _x =	5.15	in ³	S _y =	5.15	in ³
r _× =	2.39	in	r _y =	2.39	in
COLUMN HT (I) =	14.50	ft	K =	2.10	
LOAD CASE 2					
D + L =	TVL				
D+L=	5,981.67	lb			
D+L-	3,801.07	טו			
M =	NONE				
M =	0.00	ft-lb			
•••	0.00				
f _e =	TVL/A		f _b =	M/S	
f _e =	2,215.43	psi	f _b =	0.00	
- u	_,	F			
KI/r =	152.89				
F _a =	6,389.04	psi	F₀□	22,000.00	psi
fa/Fa +/- fb/Fb ≤	1.00				
fa/Fa + fb/Fb =	0.35	OK			
fa/Fa - fb/Fb =	0.35	OK			

M-C TOYOTA OF CARLSBAD

SHEET:<u>14</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

STRONG DIRECTION

LOAD CASE 3

D+(W or E/1.4) =	D + E/1.4				
D = D =	TDL 1,196.33	lb	VERTICAL LOAD		
E/1.4	427.26	lb	HORIZONTAL LOAD		
M = M =	(E/1.4)*I 6,195.30	ft-lb			
f _a = f _a =	TDL/A 443.09	psi	f _b = f _b =	M/S 14,435.64	psi
KI/r =	152.89				
F _a =	6,389.04	psi	F _b =	22,000.00	psi
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.33 0.73 -0.59	DUE TO OK OK	LATERAL		

LOAD CASE 5 GOVERNS

D + .75*[L+(W or	D + .75*L + .75*(E/1.4)	
D =	TDL	
D =	1,196.33	lb
.75*L =	.75*TLL	
.75*L =	3,589.00	lb
VL =	D+.75*L	
VL =	4,785.33	lb
.75*(E/1.4) =	.75*(E/1.4)	
.75*(E/1.4) =	320.45	lb
M =	(.75*(E/1.4))*I	
M =	4,646.47	ft-lb

M-C TOYOTA OF CARLSBAD

SHEET:<u>15</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

STRONG DIRECTION

LOAD CASE 5

 $f_a = VL/A$ $f_b = M/S$ $f_a = 1,772.35$ psi $f_b = 10,826.73$ psi

KI/r = 152.89

 $F_a = 6,389.04$ psi $F_b = 22,000.00$ psi

fa/Fa +/- fb/Fb ≤ 1.33 DUE TO LATERAL

fa/Fa + fb/Fb = 0.77 OK fa/Fa - fb/Fb = -0.21 OK

WEAK DIRECTION

LOAD CASE 1

D D = TDL

DOES NOT GOVERN LESS THAN LOAD CASE 2

LOAD CASE 2

D + L

D+L= TVL

LOAD CASE 3

D+(W or E/1.4)

D+(W or E/1.4) = D + W

LOAD CASE 4

.9D +/- E/1.4

.9D +/- E/1.5 = .9D +/- E/1.4 DOES NOT GOVERN LESS THAN LOAD CASE 3

LOAD CASE 5

D + .75*[L+(W or E/1.4)]

 $D + .75^{*}[L+(W \text{ or } E/1.4)] = D + .75^{*}L + .75^{*}W$

TRY A HSS 6 X 6 X 1/8

in² 2.70 A = in3 in³ S_x = 5.15 $S_v =$ 5.15 $r_{x} =$ 2.39 $r_v =$ 2.39 in in K = 2.10 COLUMN HT (I) = 14.50 ft

LOAD CASE 2

D + L = TVL D + L = 5,981.67 lb

M-C TOYOTA OF CARLSBAD

SHEET: 16OF: 42 JOB NO:04D141 DATE:6/8/2004BY:DKR

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ALT. COLUMN

WEAK DIRECTION

LUAD CASE Z							
M =	NONE						
M =	0.00	ft-lb					
f _a =	TVL/A		f _b =	M/S			
f _a =	2,215.43	psi	f _b □	0.00			
KI/r =	152.89						
F _a =	6,389.04	psi	F _b =	22,000.00	psi		
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.00 0.35 0.35	OK OK					
LOAD CASE 3							
D+(W or E/1.4) =	D + E/1.4						
. D=	TDL						
D =	1,196.33	lb	VERTICAL LOAD				
E/1.4 =	427.26	lb	HORIZONTAL LOAI)			
M =	(E/1.4)*I						
M =	6,195.30	ft-lb					
f _a =	TDL/A		f _b =	M/S			
f _a =	443.09	psi	f _b =	14,435.64	psi		
KI/r =	152.89						
F _a =	6,389.04	psi	F _b =	22,000.00	psi		
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.33 0.73 -0.59	DUE TO OK OK	LATERAL				
LOAD CASE 5	GOVERNS						
D + .75*[L+(W or E/1.4)] =		D + .75*L + .75*(E/1.4)					

D +
$$.75*[L+(W \text{ or E}/1.4)] = D + .75*L + .75*(E/1.4)$$

M-C TOYOTA OF CARLSBAD

SHEET:<u>17</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

WEAK DIRECTION

LOAD CASE 5

D = D =	TDL 1,196.33	lb			
.75*L = .75*L =	.75*TLL 3,589.00	lb			
VL = VL =	D+.75*L 4,785.33	lb			
.75*(E/1.4) = .75*(E/1.4) =	.75*(E/1.4) 320.45	lb			
M = M =	(.75*(E/1.4))*I 4,646.47	ft-lb			
f _e =	VL/A		f _b =	M/S	
f _a =	1,772.35	psi	$f_b =$	10,826.73	psi
Kl/r □	152.89				
F _a =	6,389.04	psi	F _b =	22,000.00	psi
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.33 0.77 -0.21	DUE TO OK OK	LATERAL		

FOOTING

LATERAL

TRY 24" DIAMETER BY 5'-0" DEEP

(2.34*P)/S₁*b A = A/2 * (1+ SQRT(1 + (4.36*h)/A))) d = 427.26 GOVERNING LATERAL LOAD P = PASSIVE = 100.00 DEPTH = 5.00 $S_1 =$ 166.67 DIAMETER = 2.00 ft **b** = 2.00 ft ft HEIGHT(h) = 14.50

FOOTING
24" DIAMETER BY
5'-0" DEEP
EMBED COLUMN
4'-0"
OK FOR TOTAL
LOAD
OK FOR UPLIFT

M-C TOYOTA OF CARLSBAD

SHEET:<u>18</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

FOOTING						
A =	1.12					
d =	4.82	OK				
TOTAL LOAD						
Trib. Width (TW) =	18.50	ft	Dead Load (DL) =	4.00	psf	
Length (L) =	16.17	ft	Live Load (LL) =	16.00	psf	
Trib. Area (TA) =	299.08	ft²	Total Load (TL) =	20.00	psf	
TOTAL DOWNWA	RD LOAD (T	DL) =	TL*TA			
TDL =	5,981.67	lb				
SKIN FRICTION (S	SK) =	CIRCUM	FERENCE OF FOOTIN	NG * FRICT	TON WITH S	OIL
SK =	5,235.99	lb				
END BEARING (B)) =	END ARE	EA OF THE FOOTING	* SOIL BE/	ARING VALU	ΙE
SOIL BEARING VA	ALUE =	1,000.00	psf			
B =	3,141.59	lb				
B+SK =	8,377.58	>	5,981.67	TDL	OK	
UPLIFT						
UPLIFT (U) =	P∪*TA					
U = ` _	2,796.19	lb				
RESISTING DEAD	LOAD (RDL)=	DL*TA			
RDL=	1,196.33	ĺb				
CONCRETE WT (CWT) =	VOLUME	OF CONCRETE * WT	Γ		
CWT =	2,356.19					
SK =	5,235.99	lb				
RDL+CWT+SK =	8,788.52	>	2,796.19	U	ок	

M-C TOYOTA OF CARLSBAD

SHEET:<u>19</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:6/8/2004BY:DKR

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CONNECTIONS

PURLIN TO BEAM

PURLIN $V_L = V_R = 2,018.81$

USING 2 BOLTS

 $Ib/BOLT = V_{L-OR-R}/2$

Ib/BOLT = 1,009.41 lb

lb

USE 2 - 1/2" DIAMETER A307 BOLTS

OR

BEAM $V_L = V_R = 2,018.81$ lb

USING #12 SCREWS

ALLOWABLE #12(V_A) = 657.00 lb

OF SCREWS (n) = $V_L N_A$

n = 3.07

USE 4 - # 12 SCREWS EACH BEAM TO COLUMN

BEAM TO COLUMN

BEAM $V_L = V_R = 5,981.67$ lb

USING 2 BOLTS

 $Ib/BOLT = V_{L-OR-R}/2$

Ib/BOLT = 2,990.83 Ib

USE 2 - 1/2" DIAMETER A307 BOLTS

OR

BEAM $V_1 = V_R = 5,981.67$ lb

USING #12 SCREWS

ALLOWABLE #12(V_A) = 657.00 lb

OF SCREWS (n) = V_L/V_A

n = 9.10

USE 10 - # 12 SCREWS EACH BEAM TO COLUMN

PURLIN TO BEAM
2- 1/2" DIAMETER
A307 BOLTS
OR 4 - #12
SCREWS
EACH PURLIN TO
EACH BEAM W/ A
12 GA. CLIP
ANGLE

BEAM TO COLUMN

2- 1/2" DIAMETER
A307 BOLTS
OR 10 - #12
SCREWS
EACH BEAM
TO EACH
COLUMN

M-C TOYOTA OF CARLSBAD

SHEET:<u>20</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:6/8/2004BY:DKR

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CONNECTIONS

BEAM TO BUILDING

BEAM TO CLIP

BEAM $V_L = V_R = 5,981.67$ lb USING 2 BOLTS lb/BOLT = $V_{L-OR-R}/2$

lb/BOLT = 2,990.83 lb USE 2 - 1/2" DIAMETER A307 BOLTS

OR

BEAM V_L=V_R= 5,981.67 lb

USING #12 SCREWS

ALLOWABLE #12(V_A) = 657.00 lb

OF SCREWS (n) = $V_L N_A$

n = 9.10

USE 10 - # 12 SCREWS EACH BEAM TO COLUMN

CLIP TO WALL

BEAM $V_L = V_R = 5,981.67$ lb

KWIK BOLT-II

ALLOWABLE $5/8"(V_A) = 3,125.00$ lb

OF BOLTS (n) = $V_L N_A$

n = 1.91 ft

USE 2 - 5/8" DIAMETER KWIK BOLT-II W/ 4" EMBEDMENT INTO THE WALL

OWNER TAKES RESPONSIBILITY FOR ADEQUACY OF BUILDING WALL TO CARRY ADDITIONAL LOADS

BEAM TO BUILDING

BEAM TO CLIP
2- 1/2" DIAMETER
A307 BOLTS
OR 10 - #12
SCREWS
EACH BEAM
TO EACH
12 GA. CLIP
ANGLE

CLIP TO WALL
2 - 5/8" DIAMETER
KWIK BOLT -II W/
4" EMBEDMENT
INTO EXST.
WALL

NOTE:
OWNER TAKES
RESPONSIBILITY
FOR ADEQUACY
OF BUILDING
WALL TO CARRY
ADDITIONAL
LOADS

M-C TOYOTA OF CARLSBAD

SHEET:<u>21</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

STRUCTURAL ENGINEER 1046 CALLE RECODO SUITE J SAN CLEMENTE, CA 92673 PHONE (949)492-5981 FAX (949)498-3020

CONNECTIONS

DECK PULLOUT

P_U= 9.35

psf

P_{U-EFFECTIVE} = P_U-ROOF DL

P_{U-EFFECTIVE}= 9.35 psf

w= P_{U-EFFECTIVE}*TW

w= 75.57 plf

SCREWS PER FOOT= w/PULLOUT

PULLOUT = 349.00 lb

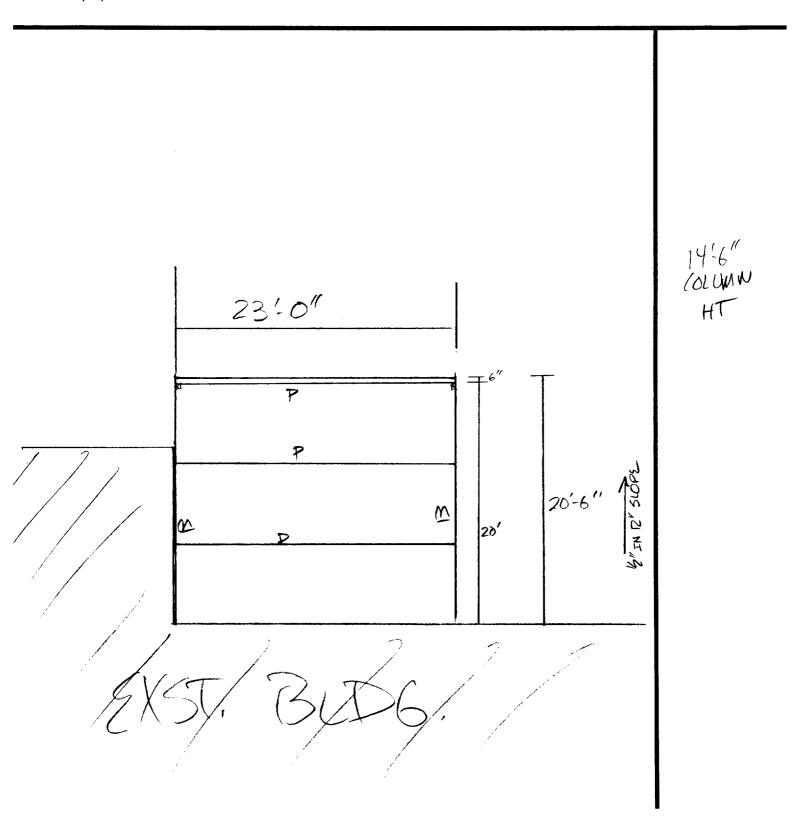
SCREWS PER FOOT= 0.22

SCREWS PER 15" = 0.27

USE 1-#10 SMS EVERY 15 "

DECK PULLOUT 1-#10 EVERY 15" INTO EACH PURLIN

M-C TOYOTA OF CARLSBAD SHEET:<u>22</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>



M-C TOYOTA OF CARLSBAD

SHEET:<u>23</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

Dead Loads						
Roof Deck	1.00	psf				
Purlins	1.50	psf				
Beam	1.50	psf				
Total	4.00	psf	_			
B 11						750/41/0
<u>Decking</u>						<u>DECKING</u> HR-36 AEP 26
						GAUGE
SIMPLE SPAN						GAUGE
Trib. Width (TW) =	1.00	ft	Dead Load (DL) =	1.00	psf	
Length (L) =	6.67	ft	Live Load (LL) =	20.00	psf	
F _b =	50,000.00	psi	Total Load (TL) =	21.00	psf	
• b	00,000.00	poi	Total Load (TL)	2.1.00	рог	
w = TL*TW =	21.00	plf				
M= (w*L²)/8 =	116.67	ft-lb				
•						
$S_{req} = M/F_b =$	0.0280	in ³ /ft				
Use HR-36 AEP 26	gauge	S=	0.0895	in ³ /ft	OK	
CANTILEVER SPAN						
Tolk \8/(dth /T\8/\ -	4.00	£	Dond Lond (DL) =	4.00	af	
Trib. Width (TW) = Length (L) =	1.00 0.50	ft ft	Dead Load (DL) = Live Load (LL) =	1.00 20.00	psf psf	
Length (L) -	50,000.00	psi	Total Load (TL) =	21.00	psi psf	
' ь	30,000.00	þsi	Total Load (TL) -	21.00	þsi	
w = TL*TW =	21.00	plf				
		•				1
$M = (w^*L^2)2 =$	2.63	ft-lb				
S _{req} □ M/F _b =	0.0006	in³/ft	SIMPLE SPAN GOVE	ERNS		
<u>PURLINS</u>						PURLINS
						9 C 12 X 3 AEP
Trib. Width (TW) =	6.67	ft	Dead Load (DL) =	2.50	psf	OR
Length (L) =	23.00	ft	Live Load (LL) =	20.00	psf	10 C 12 X 2.5 AEP
Trib. Area (TA) =	153.33	ft²	Total Load (TL) =	22.50	psf	OR
_						10 C 12 X 2.5
F _b	30,000.00	psi				POWERS
- The shows & a	450.00					
w = TL*TW =	150.00	plf				1
						Ī

M-C TOYOTA OF CARLSBAD

SHEET:24OF:42 JOB NO:04D141 DATE:6/8/2004BY:DKR

PURLINS						
$V_L = V_R = (w^*L)/2 =$	1,725.00	lb				
M= (w*L ²)/8 =	9,918.75	ft-lb				
$S_{req} = M/F_b =$	3.9675	in ³				
Use 9C12X3 AEP OR		S=	4.3260	in ³	ОК	
Use 10C12X2.5 AEI OR	P	S=	4.6850	in ³	OK	
Use 10C12X2.5 PO	WERS	S=	4.7200	in ³	OK	
BEAM						BEAM
Trib. Width (TW) □	11.50	ft	Dead Load (DL) =	4.00	psf	10 C 12 X 2.5 AEP OR 10 C 12 X 2.5
Length (L) =	20.00	ft	Live Load (LL) =	16.00	psf	POWERS
Trib. Area (TA) =	230.00	ft²	Total Load (TL) =	20.00	psf	
F _b =	30,000.00	psi			•	
w = TL*TW =	230.00	plf				
V_L OR V_R = (w*L)/2 =	2,300.00	lb				
$M = (w^*L^2)/8 =$	11,500.00	ft-lb				
$S_{req} = M/F_b =$	4.6000	in ³				
Use 10C12X2.5 AE OR	Р	S=	4.6850	in ³	ОК	
Use 10C12X2.5 PO	WERS	S=	4.7200	in ³	OK	

M-C TOYOTA OF CARLSBAD

SHEET:<u>25</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

COLUMN		-				COLUMN
VERTICAL LOADS	1					2 - 10 C 12 X 3.25 AEP WELDED TOGETHER
Trib. Width (TW) =		ft	Dead Load (DL) =	4.00	psf	POOLITIER
Length (L) =	10.50	ft	Live Load (LL) =		psf	
Trib. Area (TA) =		ft²	Total Load (TL) =		psf	
F _y =	55,000.00	psi	F _b =	30,000.00	psi	
Total Dead Load (TDL =	TDL) = 483.00	DL*TA Ib				
Total Live Load (T	LL) =	LL*TA				
TLL =	2,415.00	lb				
Total Vertical Load TVL =	i (TVL) = 2,898.00	TDL+TLL lb				
WIND LOAD	70 MPH EXP	. C				
P =	$q_s^*C_e^C_q^l_w$					
	$q_s =$	12.60				
	C° =	1.06				
	C _a =	1.30	horizontal	0.70	upward	
	I _w =	1.00				
P _H =	17.36	psf				
P _U =	9.35	psf				
HEIGHT OF ROO	F (H) =	SI OPF *	LENGTH (L)			
SLOPE	1/24	L =	20.50	ft		
H=	0.85	ft				
Trib. Width (TW) =		ft	Dead Load (DL) □	4.00	psf	
Trib. Length (L) =	10.50	ft	Live Load (LL) =	20.00	psf	
Trib. Area (TA) =	120.75	ft ²	Total Load (TL) =	24.00	psf	
F _b =	22,000.00	psi	COLUMN HT (CH) =	14.50	ft	
NUMBER OF COL	_UMNS (n) =	2.00				
WIND FORCE (W) =	P _H *H*TW/r	ı			
W =	85.28	lb				

M-C TOYOTA OF CARLSBAD

SHEET:<u>26</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

STRUCTURAL ENGINEER 1046 CALLE RECODO SUITE J SAN CLEMENTE, CA 92673 PHONE (949)492-5981 FAX (949)498-3020

COLUMN

)AD

SCISIVIC LOAD					
ZONE =	4.00		DESIGN BASE SHEAR		
C _a =	0.44		$V = (C_v^*I^*W)/(R^*T) =$	2.25	*W
C _v =	0.77		V =	1,086.89	lb
R =	2.20				
l =	1.00		MAX DESIGN SHEAR		
h _n =	15.35		$V = (2.5 C_a^*I^*W)/(R) =$	0.50	*W
$C_t =$	0.02		V =	241.50	lb
T =	0.16				
N _a =	1.00	MIN	DESIGN SHEAR (ZON	IE 4)	
N _v =	1.20	\	$/ = (.8*Z*N_v*I*W)/(R) = $	0.17	*W
Z =	0.40		V =	84.31	lb
Soil Profile Type	Sd				
Seismic Source =	В				
Distance To Source =	≥ 5 km				
Trib. Width (TW) =	11.50	ft	Dead Load (DL) =	4.00	psf
Length (L) =	10.50	ft	Live Load (LL) =	20.00	psf
Trib. Area (TA) =	120.75	ft ²	Total Load (TL) =	24.00	psf
, ,			COLUMN HT (CH) =	14.50	· ft
10/ -	DI *TA				
W = W =	DL*TA 483.00	lb			
VV	463.00	เถ			
V _{TOTAL} =	943.00	lb	A _B =	471.50	ft²
r _{mex} =	V/V _{TOTAL}				
r _{max} =	0.26				
ρ = 2	2-((20)/(r _{max} *so	irt(A ₂)))			
ho =	1.00	' '\ 'B///			
\rangle -	1.00				
E =	ρ *V				
E =	241.50	lb			
E/1.4 =	172.50	lb			

M-C TOYOTA OF CARLSBAD

SHEET:<u>27</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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COLUMN

LUMN	- · · · · · · ·				
STRONG DIRECTIO	<u>N</u>				
LOAD CASE 1					
D D=	TDL		DOES NOT GOVE	ERN LESS THAN	LOAD CASE 2
LOAD CASE 2					
D+L D+L=	TVL				
LOAD CASE 3	1 4 2				
D+(W or E/1.4)	D . E// 4				
D+(W or E/1.4) = LOAD CASE 4	D + E/1.4				
.9D +/- E/1.4					
.9D +/- E/1.5 =	.9D +/- E/1.4		DOES NOT GOVE	ERN LESS THAN	LOAD CASE 3
<u>LOAD CASE 5</u> D + .75*[L+(W or E	5/1 4 \1				
D + .75*[L+(W or E		D + .75*	'L + .75*(E/1.4)		•
TRY 2 - 10 C 12 X	2.05 AED				
A=	3.25 AEP 2.59	in ²			
S _x =	11.05	in ³	S _y =	2.38	in ³
r _x =	7.71	in	r _y =	2.41	in
COLUMN HT (I) =		ft	, K =	2.10	
LOAD CASE 2					
D+L=	TVL				
D + L =	2,898.00	ib			
M =	NONE				
M =	0.00	ft-lb			
f _a =	TVL/A		f _b =	M/S	
f _e =	1,119.78	psi	f _b =	0.00	
' a	1,110.70	ры	•6	0.00	
KI/r =	47.38				
F _a =	24,752.89	psi	F _b =	30,000.00	psi
fa/Fa +/- fb/Fb ≤	1.00				
fa/Fa + fb/Fb =	0.05	OK			
fa/Fa - fb/Fb =	0.05	OK			

M-C TOYOTA OF CARLSBAD

SHEET:<u>28</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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COLUMN

STRONG DIRECTION

LUAD CASE 3					
D+(W or E/1.4) =	D + E/1.4				
D = D =	TDL 483.00	lb	VERTICAL LOAD		
E/1.4 =	172.50	lb	HORIZONTAL LOAD)	
M = M =	E/1.4*I 2,501.25	ft-lb			
f _e =	TDL/A		f _b =	M/S	
f _e =	186.63	psi	$f_b =$	2,715.31	psi
KI/r =	47.38				
F _a =	24,752.89	psi	F _b =	30,000.00	psi
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =		DUE TO OK OK	LATERAL		
LOAD CASE 5	GOVERNS				
D + .75*[L+(W or E	E/1.4)] =	D + .75*	L + .75*(E/1.4)		
D = D =	TDL 483.00	lb			
.75*L = .75*L =	.75*TLL 1,811.25	lb			
VL = VL =	D+.75*L 2,294.25	lb			
.75*(E/1.4) = .75*(E/1.4) =	.75*(E/1.4) 129.38	lb			
M = M =	.75*((E/1.4)*I) 1,875.94	ft-lb			

M-C TOYOTA OF CARLSBAD

SHEET:<u>29</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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CO	L	Ū	Jŧ	И	N

STRONG DIRECTION

LOAD CASE 5

f _a =	VL/A		$f_b =$	M/S	
f _a =	886.50	psi	f _b =	2,036.48	psi

KI/r = 47.38

 $F_a = 24,752.89$ psi $F_b = 30,000.00$ psi

fa/Fa +/- fb/Fb ≤ 1.33 DUE TO LATERAL

fa/Fa + fb/Fb = 0.1037 OK fa/Fa - fb/Fb = -0.03 OK

WEAK DIRECTION

LOAD CASE 1

D = TDL DOES NOT GOVERN LESS THAN LOAD CASE 2

LOAD CASE 2

D + L

D+L=TVL

LOAD CASE 3

D+(W or E/1.4)

D+(W or E/1.4) = D + E/1.4

LOAD CASE 4

.9D +/- E/1.4

.9D +/- E/1.5 = .9D +/- E/1.4 DOES NOT GOVERN LESS THAN LOAD CASE 3

LOAD CASE 5

D + .75*[L+(W or E/1.4)]

D + .75*[L+(W or E/1.4)] = D + .75*L + .75*(E/1.4)

TRY 2 - 10 C 12 X 3.25 AEP

in² A = 2.59 in in³ 2.38 $S_v =$ 11.05 $S_x =$ 2.41 in $r_v =$ 7.71 $r_x =$ in K = 2.10 ft COLUMN HT (I) = 14.50

LOAD CASE 2

D + L = TVLD + L = 2,898.00 lb

M-C TOYOTA OF CARLSBAD

SHEET:30OF:42 JOB NO:04D141 DATE:6/8/2004BY:DKR

STRUCTURAL ENGINEER 1046 CALLE RECODO SUITE J SAN CLEMENTE, CA 92673 PHONE (949)492-5981 FAX (949)498-3020

COLUMN

WEAK DIRECTION

M =	NONE				
M =	0.00	ft-lb			
f _a =	TVL/A		£	MIC	
-			f _b =	M/S	
f _a =	1,119.78	psi	f _b =	0.00	
KI/r =	151.87				
F _e =	6,471.67	psi	F _b =	30,000.00	psi
fa/Fa +/- fb/Fb ≤	1.00				
fa/Fa + fb/Fb =	0.17	OK			
fa/Fa - fb/Fb =	0.17	OK			
LOAD CASE 3					
D+(W or E/1.4) =	D + E/1.4				
D =	TDL				
D =	483.00	lb	VERTICAL LOAD		
				_	
E/1.4 =	172.50	lb	HORIZONTAL LOAD)	
M =	E/1.4*I				
M =	2,501. 2 5	ft-lb			
			_		
f _a =	TDL/A		f _b =	M/S	
f _a =	186.63	psi	f _b =	12,600.76	psi
KI/r =	151.87				
F _a =	6,471.67	psi	F _b =	30,000.00	psi
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb =		DUE TO	LATERAL		
fa/Fa - fb/Fb =	-0.39	OK			
LOAD CASE 5	GOVERNS				
D + .75*[L+(W or		D + .75*	L + .75*(E/1.4)		
• '			•		

M-C TOYOTA OF CARLSBAD

SHEET:310F:42 JOB NO:04D141 DATE:6/8/2004BY:DKR

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COLUMN

WEAK DIRECTION

fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.33 0.4520 -0.18	DUE TO L OK OK	ATERAL		
F _e =	6,471.67	psi	F _b =	30,000.00	psi
KI/r =	151.87				
f _a =	886.50	psi	$f_b =$	9,450.57	psi
f _a =	VL/A		f _b =	M/S	
M =	1,875.94	ft-lb			
M =	.75*(E/1.4)*I				
.75*(E/1.4) = .75*(E/1.4) =	.75⁻(E/1.4) 129.38	lb			
75*(5(4.4) =	75*(514.4)			,	
VL =	2,294.25	ĺb			
VL =	D+.75*L				
.75*L =	1,811.25	lb			
.75*L =	.75*TLL				
D =	483.00	lb			
D =	TDL				

M-C TOYOTA OF CARLSBAD

SHEET:<u>32</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

ALT. COLUMN						 ALT. COLUMN
VERTICAL LO	ADS					HSS 6 X 6 X 1/8
Trib. Width (T		ft	Dead Load (DL) =	4.00	psf	
Length (L)		ft	Live Load (LL) =		psf	
•	A) = 120.75	ft ²	Total Load (TL) =		psf	
F _y =	46,000.00	psi	F _b =	22,000.00	psi	
Total Dead Lo	oad (TDL) =	DL*TA				
TDL =	483.00	lb				
Total Live Loa		LL*TA				:
TLL =	2,415.00	lb				
Total Vertical		TDL+TLL				
TVL =	2,898.00	lb				
WIND LOA	<u>D</u> 70 MPH EXP	. C				
P =	$q_s^{\star}C_e^{}C_q^{}I_w^{}$					
	$q_s =$	12.60				
	C _e =	1.06				
	$C_q =$	1.30	horizontal	0.70	upward	
	$I_w =$	1.00				
P _H =	17.36	psf				
P _U =	9.35	psf				
HEIGHT OF F	ROOF (H) =	SI OPE *	LENGTH (L)			
SLOPE	1/24	L =	20.50	ft		
H =	0.85	ft				
Trib. Width (T	W) = 11.50	ft	Dead Load (DL) =	4.00	psf	
Trib. Length (L) = 10.50	ft	Live Load (LL) =	20.00	psf	
Trib. Area (T	A) = 120.75	ft ²	Total Load (TL) =	24.00	psf	
F _b =	22,000.00	psi	COLUMN HT (CH) =	14.50	ft	
NUMBER OF	COLUMNS (n) =	2.00				
WIND FORCE	E (W) =	P _H *H*TW/i	า			
W =	85.28	lb				

M-C TOYOTA OF CARLSBAD

SHEET:<u>33</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

SE	ISM	CI	LO	AD

<u> </u>					
ZONE =	4.00		DESIGN BASE SHEAR	l l	
C _e =	0.44		$V = (C_v^*I^*W)/(R^*T) =$	2.25	*W
C _v =	0.77		V =	1,086.89	lb
R =	2.20				
l =	1.00		MAX DESIGN SHEAR		
h _n =	15.35		$V = (2.5 C_a I W)/(R) =$	0.50	*W
$C_t =$	0.02		V =	241.50	lb
T =	0.16				
N _a =	1.00	MII	N DESIGN SHEAR (ZON	IE 4)	
N _v =	1.20		$V = (.8*Z*N_**I*W)/(R) =$	0.17	*W
Z =	0.40		V =	84.31	lb
Soil Profile Type =	S_d				
Seismic Source =	В				
Distance To Source =	≥ 5 km				
Trib. Width (TW) =	11.50	ft	Dead Load (DL) =	4.00	psf
Length (L) =	10.50	ft	Live Load (LL) =	20.00	psf
Trib. Area (TA) =	120.75	ft ²	Total Load (TL) =	24.00	psf
F _b =	22,000.00	psi	COLUMN HT (CH) =	14.50	ft
· ·	,	•	.		
W =	DL*TA				
W =	483.00	ib			
V _{TOTAL} =	943.00	lb	A _B =	471.50	ft²
TOTAL	3 13/33		· ·	.,	
r _{max} =	V/V _{TOTAL}			·	
r _{max} =	0.26				
ρ =	2-((20)/(r _{max} *s	art(A⊳)))			
$\rho =$	1.00				
•	-				
E =	ρ *V				
E =	241.50	lb			
E/1.4 =	172.50	lb			

M-C TOYOTA OF CARLSBAD

SHEET:<u>34</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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fa/Fa +/- fb/Fb ≤

fa/Fa + fb/Fb =

fa/Fa - fb/Fb =

1.00

0.17

0.17

OK

OK

ALT. COLUMN					
STRONG DIRECTION	<u>N</u>				
<u>LOAD CASE 1</u> D					
D = <u>LOAD CASE 2</u>	TDL		DOES NOT GOVE	ERN LESS THAN	I LOAD CASE 2
D+L D+L=	TVL				
LOAD CASE 3 D+(W or E/1.4)	D . E/4 4				
D+(W or E/1.4) = <u>LOAD CASE 4</u> .9D +/- E/1.4	D + E/1.4				
.9D +/- E/1.5 = LOAD CASE 5	.9D +/- E/1.4		DOES NOT GOVE	ERN LESS THAN	I LOAD CASE 3
D + .75*[L+(W or I D + .75*[L+(W or I		D + .75*	L + .75*(E/1.4)		
TRY A HSS 6 X 6	X 1/8				
A =	2.70	in ²			
S _x =	5.15	in ³	S _y =	5.15	in ³
r _× =	2.39	in	r _y =	2.39	in
COLUMN HT (i) =		ft	κ´=	2.10	
LOAD CASE 2					
D + L =	TVL				
D + L =	2,898.00	lb			
M =	NONE				
M =	0.00	ft-lb			
f _a =	TVL/A		f _b =	M/S	
f _e =	1,073.33	psi	f _b =	0.00	
Kl/r =	152.89				
F _a =	6,389.04	psi	F _b =	22,000.00	psi

M-C TOYOTA OF CARLSBAD

SHEET:<u>35</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

STRONG DIRECTION

D+(W or E/1.4) =	D + E/1.4				
D = D =	TDL 483.00	lb	VERTICAL LOAD		
E/1.4 =	172.50	lb	HORIZONTAL LOA	N D	
M = M =	E/1.4*I 2,501.25	ft-lb			
f _a = f _a =	TDL/A 178.89	psi	f _b = f _b =	M/S 5,828.16	psi
KI/r =	152.89				
F _a =	6,389.04	psi	F _b =	22,000.00	psi
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.33 0.29 -0.24	DUE TO OK OK	LATERAL		
LOAD CASE 5	GOVERNS				
D + .75*[L+(W or E	/1.4)] =	D + .75*	L + .75*(E/1.4)		

M-C TOYOTA OF CARLSBAD

SHEET:<u>36</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

STRONG DIRECTION

LOAD CASE 5

† _a =	VL/A		$t_b =$	M/S	
f _a =	849.72	psi	f _b =	4,371.12	psi
KI/r =	152 80				

$$F_a = 6,389.04$$
 psi $F_b = 22,000.00$ psi

$$fa/Fa + fb/Fb = 0.33$$
 OK $fa/Fa - fb/Fb = -0.07$ OK

WEAK DIRECTION

LOAD CASE 1

D = TDL DOES NOT GOVERN LESS THAN LOAD CASE 2

LOAD CASE 2

D + L

D+L= TVL

LOAD CASE 3

D+(W or E/1.4)

D+(W or E/1.4) = D + E/1.4

LOAD CASE 4

.9D +/- E/1.4

.9D +/- E/1.5 = .9D +/- E/1.4 DOES NOT GOVERN LESS THAN LOAD CASE 3

LOAD CASE 5

 $D + .75^{*}[L+(W \text{ or } E/1.4)]$

D + .75*[L+(W or E/1.4)] = D + .75*L + .75*(E/1.4)

TRY A HSS 6 X 6 X 1/8

A =	2.70	in ²			
S _x =	5.15	in ³	S _y =	5.15	in ³
r _x =	2.39	in	r _y =	2.39	in
COLUMN HT (I) =	14.50	ft	K =	2.10	

M-C TOYOTA OF CARLSBAD

SHEET:<u>37</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:<u>6/8/2004</u>BY:<u>DKR</u>

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ALT. COLUMN

WEAK DIRECTION

LOAD CASE 2

LOAD CASE 5	-0.24 GOVERNS	UK			
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.33 0.29	DUE TO OK OK	LATERAL		
F _a =	6,389.04	psi	F _b =	22,000.00	psi
KI/r =	152.89				
f _a =	178.89	psi	f _b =	5,828.16	psi
f _a =	TDL/A		f _b =	M/S	
M = M =	E/1.4*I 2,501.25	ft-lb			
E/1.4 =	172.50	lb	HORIZONTAL LOAD		
D = D =	TDL 483.00	lb	VERTICAL LOAD		
D+(W or E/1.4) =					
LOAD CASE 3					
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.00 0.17 0.17	OK OK			
F _a =	6,389.04	psi	F _b =	22,000.00	psi
KI/r =	152.89				
f _a =	1,073.33	psi	f _b =	0.00	
f _e =	TVL/A	II-ID	f _b =	M/S	
M = M =	NONE 0.00	ft-lb			
LUAD CASE Z					

D + $.75^{+}[L+(W \text{ or } E/1.4)] = D + .75^{+}L + .75^{+}(E/1.4)$

M-C TOYOTA OF CARLSBAD

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ALT. COLUMN

WEAK DIRECTION

LOAD CASE 5

D = D =	TDL 483.00	lb			
.75*L = .75*L =	.75*TLL 1,811.25	lb			
VL = VL =	D+.75*L 2,294.25	lb			
.75*(E/1.4) = .75*(E/1.4) =	.75*(E/1.4) 129.38	lb			
M = M =	.75*(E/1.4)*I 1,875.94	ft-lb			
f _a = f _a =	VL/A 849.72	psi	f _b = f _b =	M/S 4,371.12	2 psi
'a Kl/r =	152.89	ры	'b ⁻	4,07 1.12	. ры
F _a =	6,389.04	psi	F _b =	22,000.0	0 psi
fa/Fa +/- fb/Fb ≤ fa/Fa + fb/Fb = fa/Fa - fb/Fb =	1.33 0.33 -0.07	DUE TO OK OK	LATERAL		

FOOTING

LATERAL

TRY 24" DIAMETER BY 3'-9" DEEP

A = (2.34*P)/S₁*b **d** = A/2 * (1+ SQRT(1 + (4.36*h)/A))) P = 172.50 GOVERNING LATERAL LOAD PASSIVE = 100.00 DEPTH = 3.75 S₁ = 125.00 DIAMETER = 2.00 ft 2.00 ft b = HEIGHT(h) = 14.50ft

FOOTING
24" DIAMETER BY
3'-9" DEEP
EMBED COLUMN
2'-9"
OK FOR TOTAL
LOAD
OK FOR UPLIFT

M-C TOYOTA OF CARLSBAD

SHEET:39OF:42 JOB NO:04D141 DATE:6/8/2004BY:DKR

F001	<u>ring</u>						
	A =	0.61					
	d =	3.41	OK				
	-		• • • • • • • • • • • • • • • • • • • •				
	TOTAL LOAD						
	Trib. Width (TW) =	11.50	ft	Dead Load (DL) =	4.00	psf	
	Length (L) =	10.50	ft	Live Load (LL) =	20.00	psf	
	Trib. Area (TA) =	120.75	ft²	Total Load (TL) =	24.00	psf	
	TOTAL DOWNWAR	RD LOAD (TI	DL) =	TL*TA			
	TDL =	2,898.00	lb				
	SKIN FRICTION (SI	•		ERENCE OF FOOTI	NG * FRICT	ION WITH SOIL	
	SK =	3,926.99	lb				
	END BEARING (B)			A OF THE FOOTING	* SOIL BEA	RING VALUE	
	SOIL BEARING VA		1,000.00	psf			
	B =	3,141.59	lb	0.000.00	TDI	01/	
	B+SK =	7,068.58	>	2,898.00	TDL	ок	
	UPLIFT						
	UPLIFT (U) =	Pu*TA					
	U =	1,128.92	lb				
	RESISTING DEAD			DL*TA			
	RDL=	483.00	lb				
	CONCRETE WT (C			OF CONCRETE * WT	Ī		
	CWT =	1,767.15					
	SK =	3,926.99	lb				
	RDL+CWT+SK =	6,177.14	>	1,128.92	U	ок	
CON	NECTIONS						
	PURLIN TO BEAM						PURLIN TO BEAM
							2- 1/2" DIAMETER
	PURLIN V _L =V _R =	1,725.00	lb				A307 BOLTS
	USING 2 BOLTS						OR 4 - #12
	Ib/BOLT =	$V_{L-OR-R}/2$					SCREWS
	Ib/BOLT =	862.50	lb				EACH PURLIN TO
	USE 2 - 1/2" DIAME	TER A307 E	BOLTS				EACH BEAM W/ A
							12 GA. CLIP
	OR						ANGLE
							1

M-C TOYOTA OF CARLSBAD

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CO	NN	ECT	O	NS

PURLIN TO BEAM

PURLIN V_L=V_R=

1,725.00

lb

USING #12 SCREWS

657.00

lb

OF SCREWS (n) =

ALLOWABLE #12(V_A) =

 $V_L N_A$

n =

2.63

USE 4 # 12 SCREWS EACH BEAM TO COLUMN

BEAM TO COLUMN

BEAM V_L=V_R=

2,300.00

lb

lb

lb

USING 2 BOLTS

Ib/BOLT =

V_{L-OR-R}/2

Ib/BOLT =

1.150.00 lb

USE 2 - 1/2" DIAMETER A307 BOLTS

OR

BEAM V_I = V_R=

2,300.00

USING #12 SCREWS

ALLOWABLE #12(V_A) =

657.00

OF SCREWS (n) =

n =

 $V_L N_A$

3.50

USE 4 # 12 SCREWS EACH BEAM TO COLUMN

BEAM TO COLUMN 2- 1/2" DIAMETER A307 BOLTS OR 4- #12 **SCREWS EACH BEAM TO EACH**

COLUMN

M-C TOYOTA OF CARLSBAD

SHEET:<u>41</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:6/8/2004BY:<u>DKR</u>

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CONNECTIONS

BEAM TO BUILDING

BEAM TO CLIP

BEAM $V_L = V_R = 2,300.00$ lb

USING 2 BOLTS

 $Ib/BOLT = V_{L-OR-R}/2$

Ib/BOLT = 1,150.00 Ib

USE 2 - 1/2" DIAMETER A307 BOLTS

OR

BEAM $V_L = V_R = 2,300.00$ lb

USING #12 SCREWS

ALLOWABLE #12(V_A) = 657.00 lb

OF SCREWS (n) = $V_L N_A$

n = 3.50

USE 4 - # 12 SCREWS EACH BEAM TO COLUMN

CLIP TO WALL

BEAM $V_1 = V_R = 2,300.00$ lb

KWIK BOLT-II

ALLOWABLE $1/2"(V_A) = 1,840.00$ lb

OF BOLTS (n) = $V_L N_A$

n = 1,25 ft

USE 2 - 1/2" DIAMETER KWIK BOLT-II W/ 3.5" EMBEDMENT INTO THE WALL

OWNER TAKES RESPONSIBILITY FOR ADEQUACY OF BUILDING WALL TO CARRY ADDITIONAL LOADS

BEAM TO BUILDING

BEAM TO CLIP
2- 1/2" DIAMETER
A307 BOLTS
OR 4 - #12
SCREWS
EACH BEAM
TO EACH
12 GA. CLIP
ANGLE

CLIP TO WALL

2 - 1/2" DIAMETER KWIK BOLT -II W/ 3.5" EMBEDMENT INTO EXST. WALL

NOTE:
OWNER TAKES
RESPONSIBILITY
FOR ADEQUACY
OF BUILDING
WALL TO CARRY
ADDITIONAL
LOADS

M-C TOYOTA OF CARLSBAD

SHEET:<u>42</u>OF:<u>42</u> JOB NO:<u>04D141</u> DATE:6/8/2004BY:<u>DKR</u>

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CONNECTIONS

DECK PULLOUT

P∪=

9.35

psf

P_{U-EFFECTIVE}=

Pu-ROOF DL

P_{U-EFFECTIVE}=

8.35

psf

w=

P_{U-EFFECTIVE}*TW

w=

55.66

plf

SCREWS PER FOOT=

,

w/PULLOUT

PULLOUT =

349.00

SCREWS PER FOOT=

lb 0.16

SCREWS PER 15" =

0.20

USE 1-#10 SMS EVERY 15 "

DECK PULLOUT 1-#10 EVERY 15" INTO EACH PURLIN